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DEVELOPMENT AND CHARACTERIZATION OF COATINGS ON SELECTED METALS AND ALLOYS OBTAINED BY PLASMA ELECTROLYTIC OXIDATION

OUTLINE

- 1. INTRODUCTION**
- 2. PROBLEM FORMULATING**
- 3. PEO - SET UP**
- 4. METHODIC**
- 5. SEM, EDS, XPS, GDOES RESULTS**
- 6. OTHER SCIENTIFIC INTERESTS**

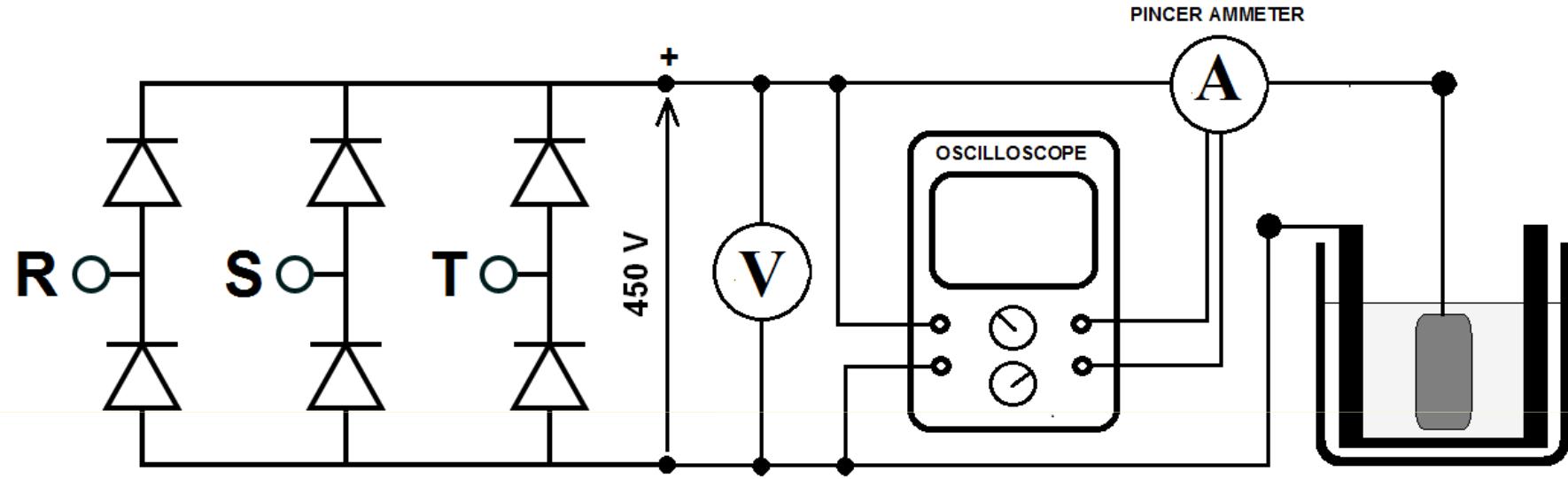
INTRODUCTION

To form the micro-coatings within micro- and nano- pores, the Plasma Electrolytic Oxidation (PEO) mainly is used. The technic is widely used by companies, such as Keronite (UK), Magoxide-Coat (Germany) and Microplasmic (USA), which are active in commercial development of PEO technology. At the beginning that method was used mainly for treatment of aluminum and its alloys. In later years, PEO was applied to oxidation of magnesium and its alloys, and titanium, and its alloys as well as niobium, zirconium and tantalum.

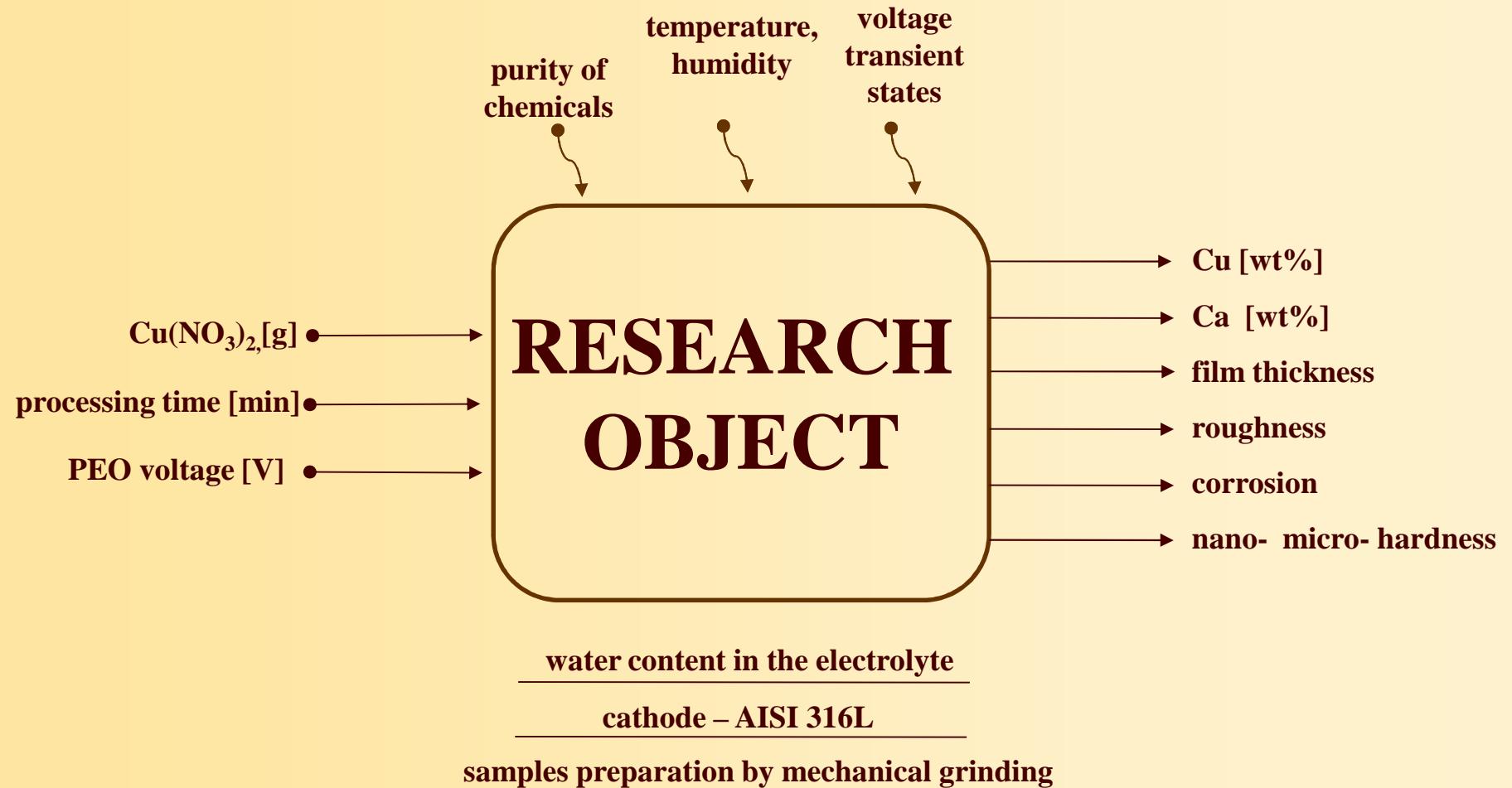
PROBLEM FORMULATING

1. Is it possible to obtain a porous coating enriched in copper on titanium and its alloys, as well as on niobium and tantalum by Plasma Electrolytic Oxidation in an electrolyte based on concentrated phosphoric acid H_3PO_4 and copper nitrate $Cu(NO_3)_2$?
2. What is the effective range of $Cu(NO_3)_2$ content in H_3PO_4 to obtain the formation of a porous coating enriched in copper of required concentration?
3. Is the copper equally distributed in the PEO coatings in whole volume?
4. Do we need the copper to be equally distributed in the first sublayer or should it go deeper into the 2nd and/or 3rd one?

PEO - SET UP



DEFINING OF OBJECT



METHOD



SCIENCE SES 2002

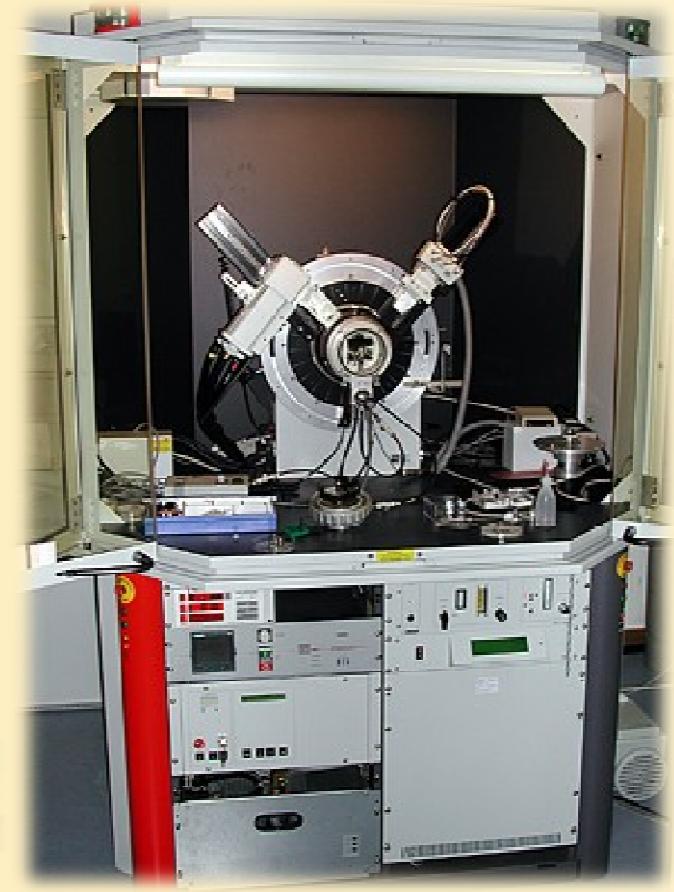


HORIBA - PROFILER 2

METHOD

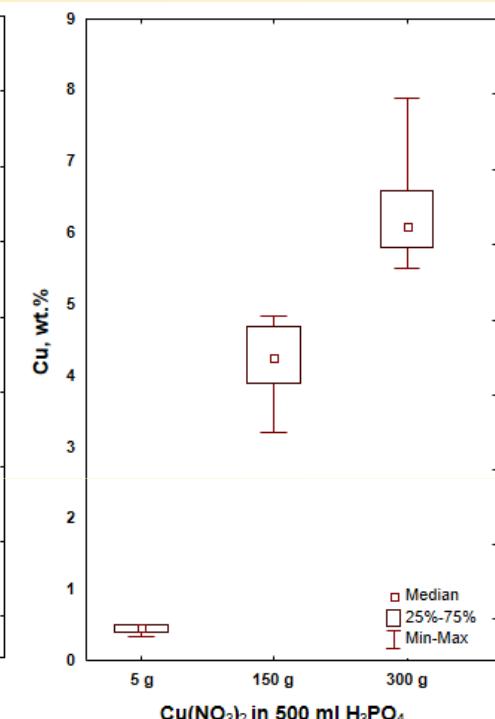
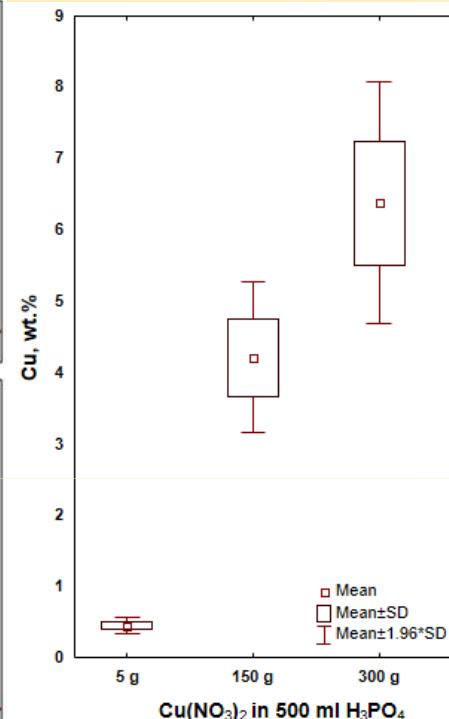
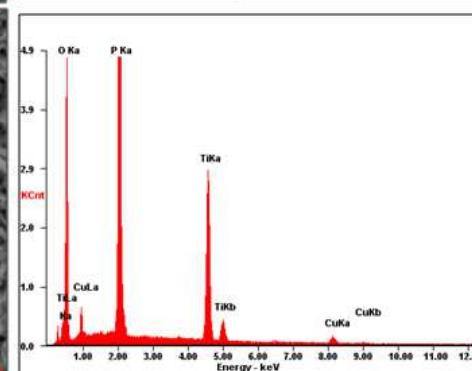
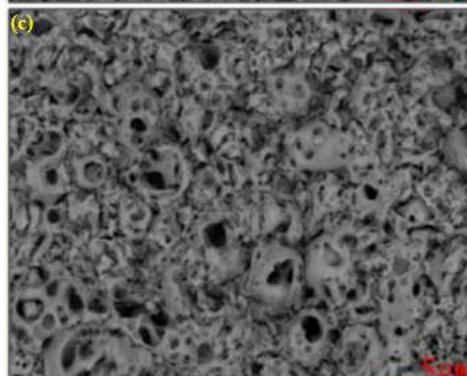
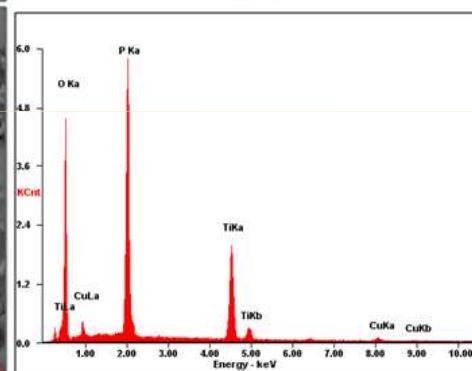
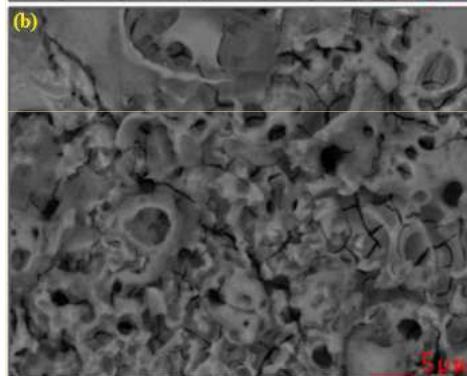
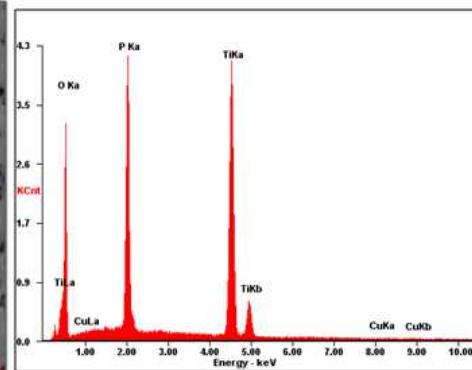
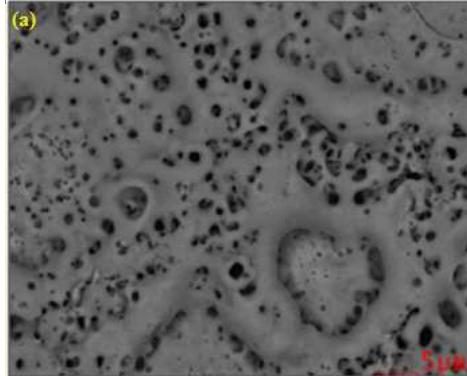


HOMMEL TESTER T800 SYSTEM
HOMMELWERKE GMBH



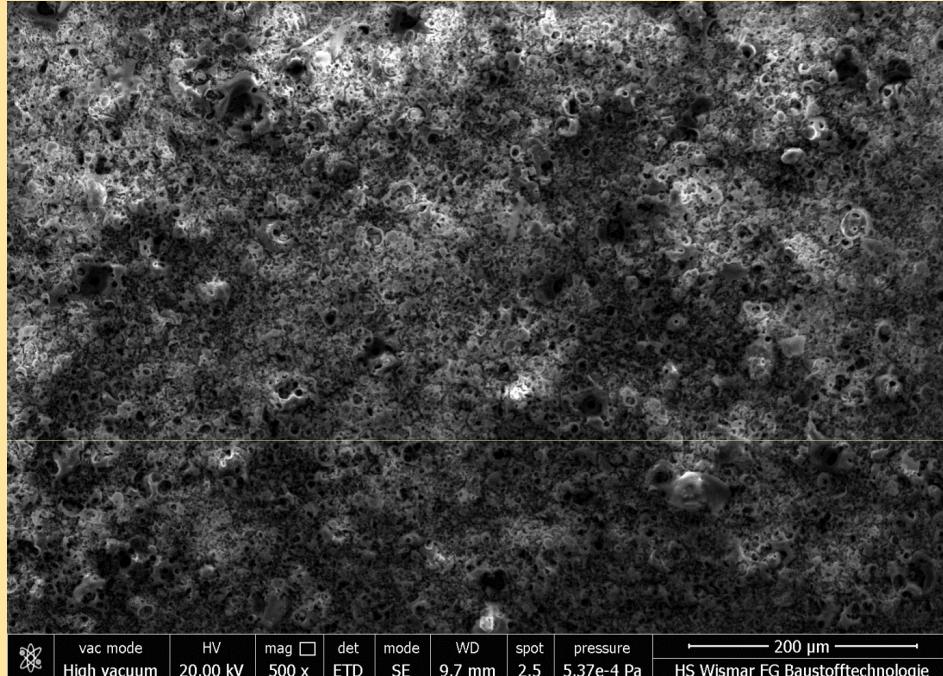
BRUKER-AXS
D8 ADVANCE

PEO - TITANIUM - SEM & EDS

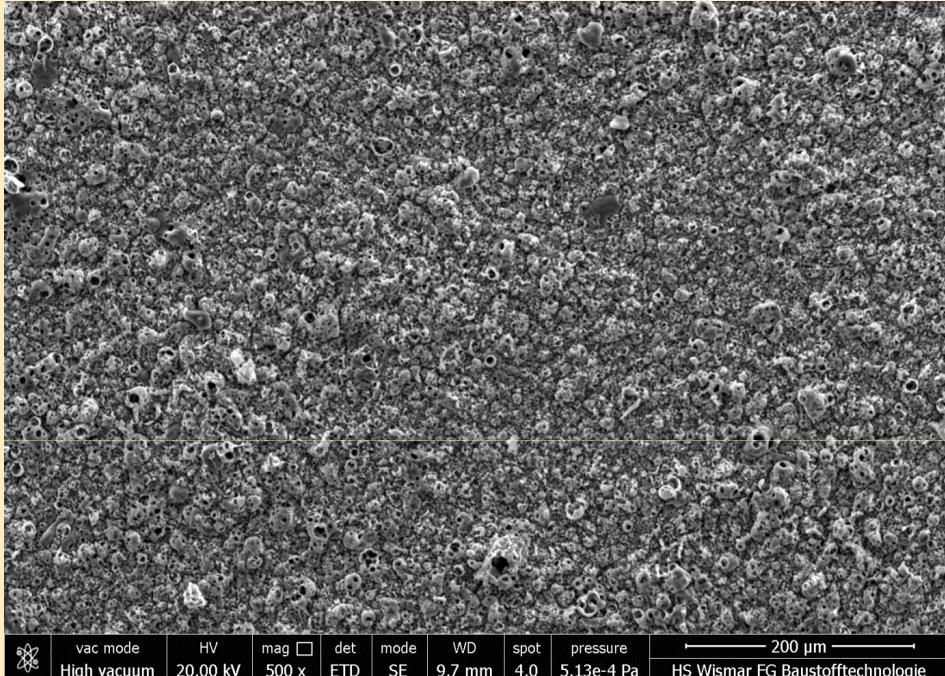


Cu, wt%	5 g Cu(NO ₃) ₂	150 g Cu(NO ₃) ₂	300 g Cu(NO ₃) ₂
Average	0.45	4.22	6.38
Variance	0.004	0.29	0.75
Standard deviation	0.06	0.54	0.86
Median	0.46	4.27	6.10
Maximum	0.51	4.85	7.9
Minimum	0.33	3.21	5.52

TITANIUM - SEM RESULTS



vac mode
High vacuum | HV 20.00 kV | mag 500 x | det ETD | mode SE | WD 9.7 mm | spot 2.5 | pressure 5.37e-4 Pa | HS Wismar FG Baustofftechnologie



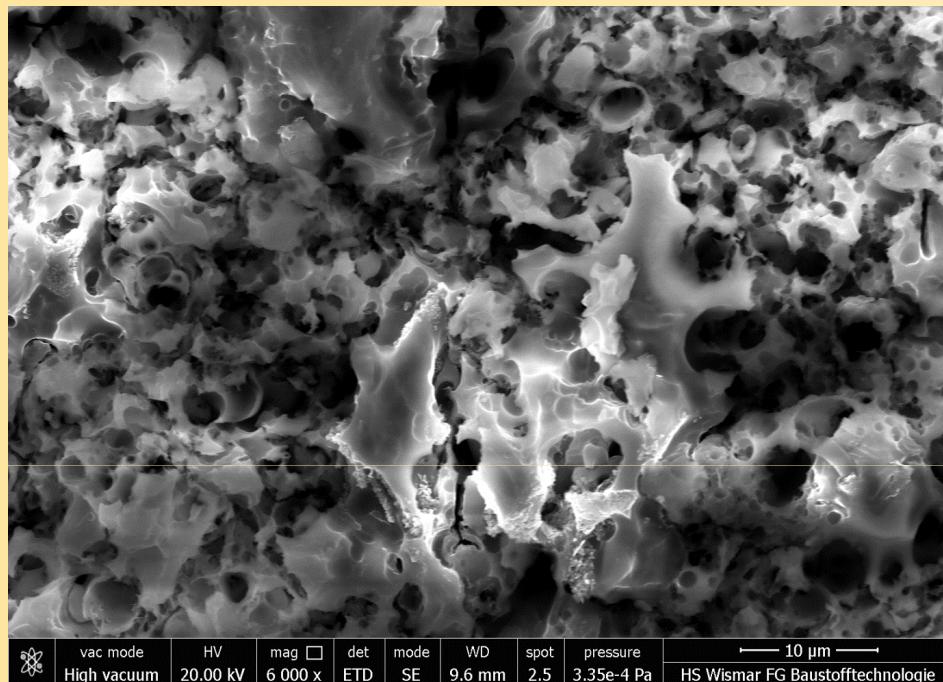
vac mode
High vacuum | HV 20.00 kV | mag 500 x | det ETD | mode SE | WD 9.7 mm | spot 4.0 | pressure 5.13e-4 Pa | HS Wismar FG Baustofftechnologie

300 g Cu(NO₃)₂ in 1 L H₃PO₄

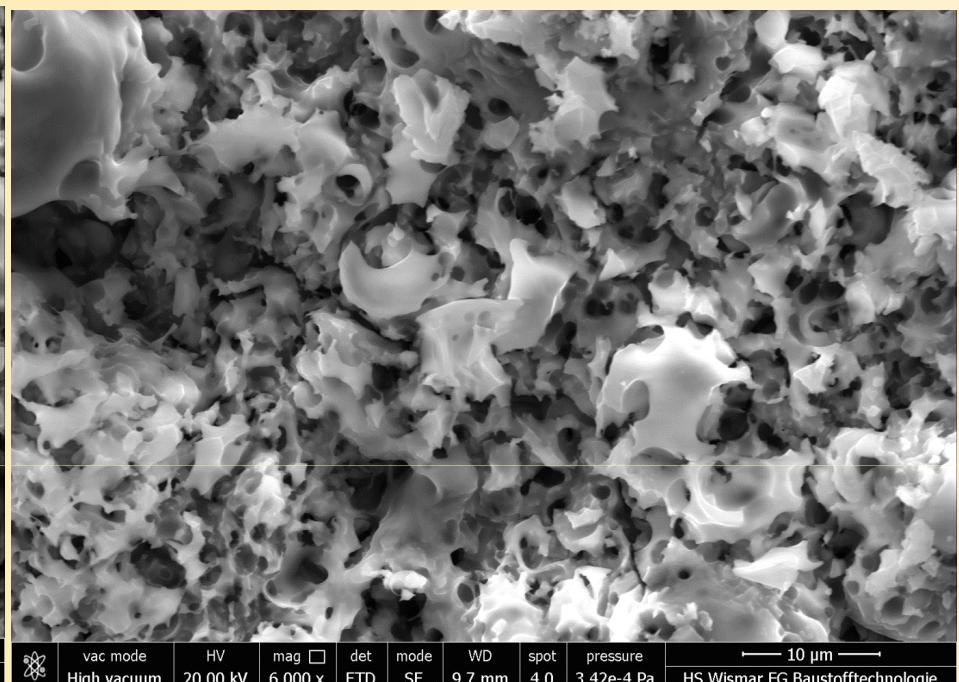
600 g Cu(NO₃)₂ in 1 L H₃PO₄

SEM pictures of porous coatings on titanium obtained by PEO
at voltage of 450 V in electrolyte containing H₃PO₄ and Cu(NO₃)₂

TITANIUM - SEM RESULTS



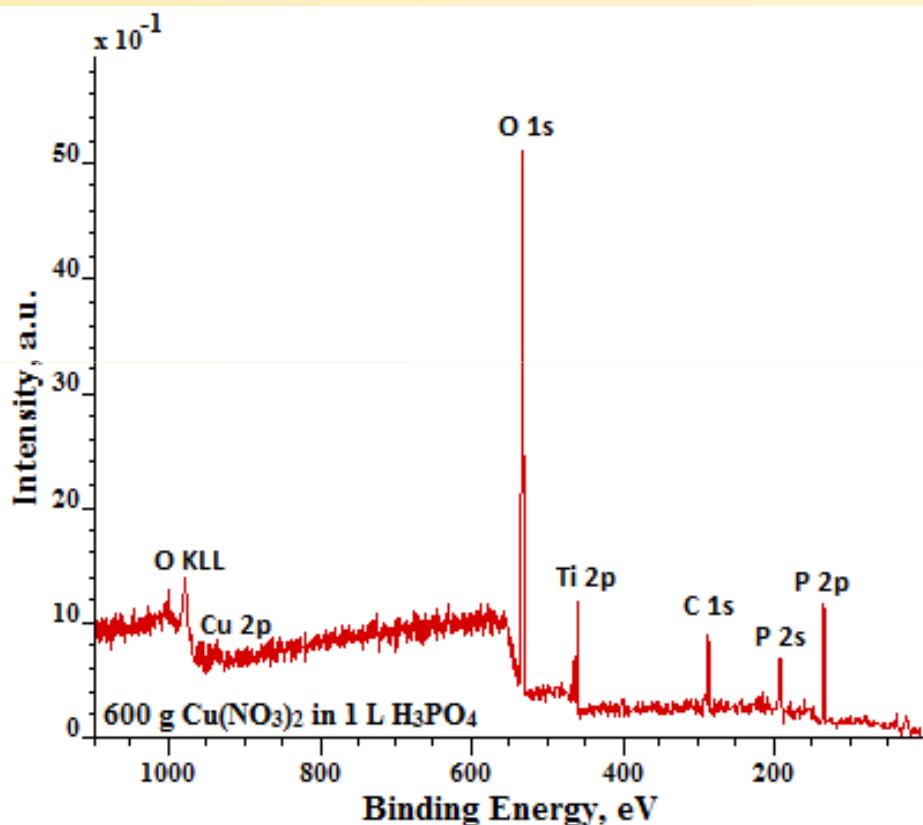
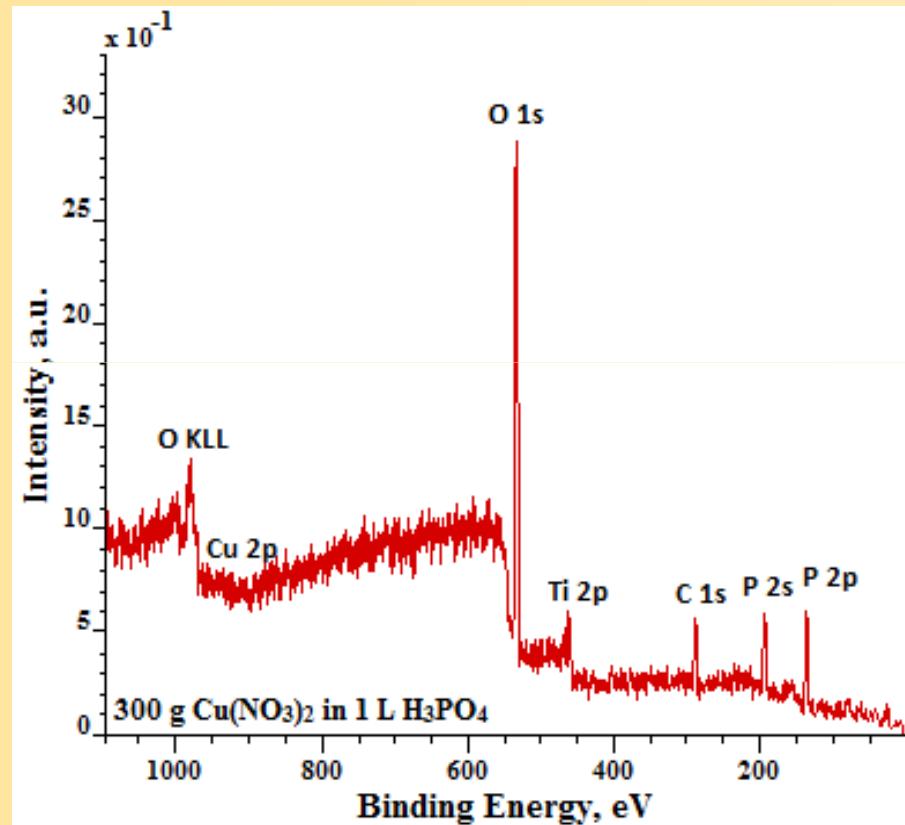
300 g Cu(NO₃)₂ in 1 L H₃PO₄



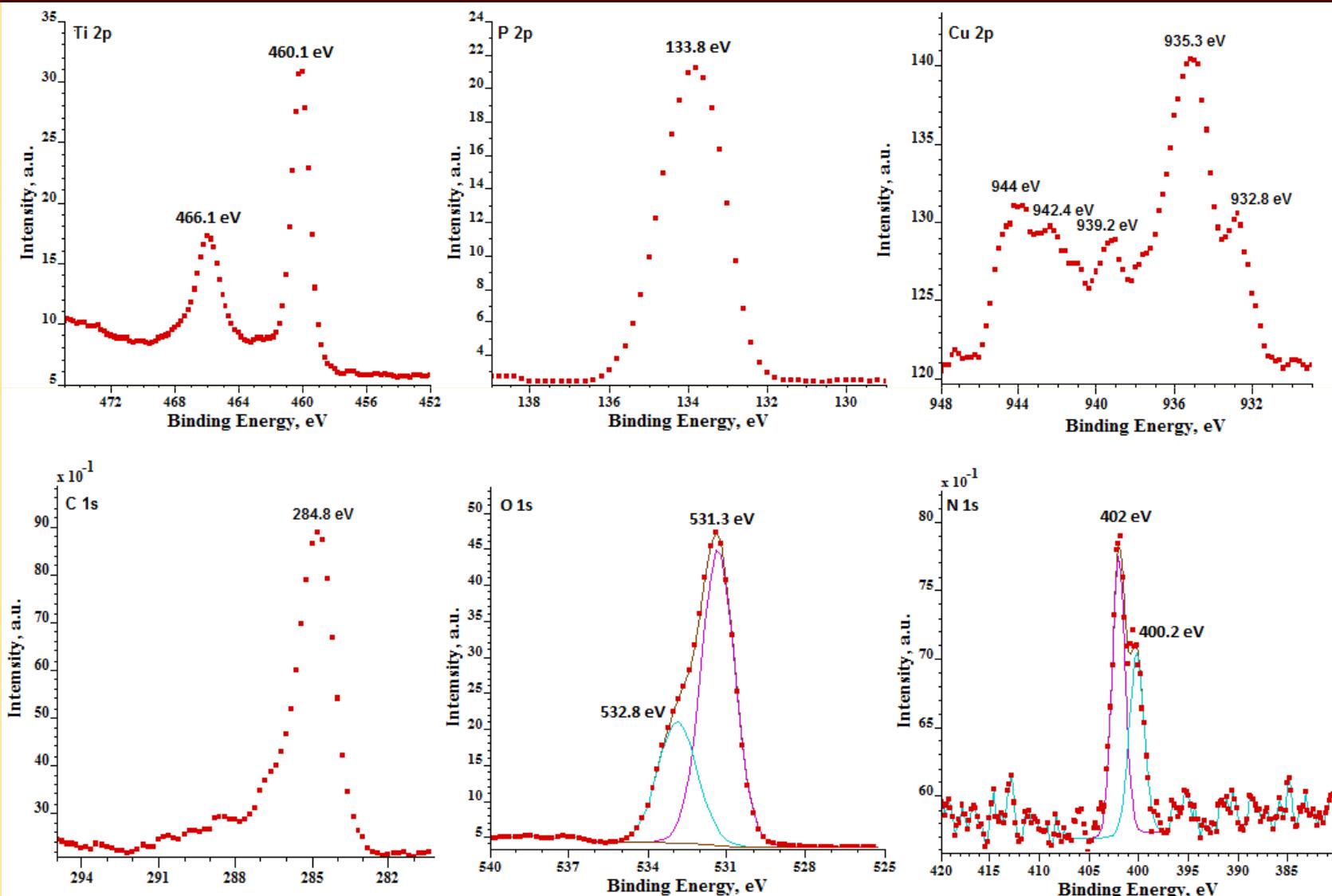
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SEM pictures of porous coatings on titanium obtained by PEO
at voltage of 450 V in electrolyte containing H₃PO₄ and Cu(NO₃)₂

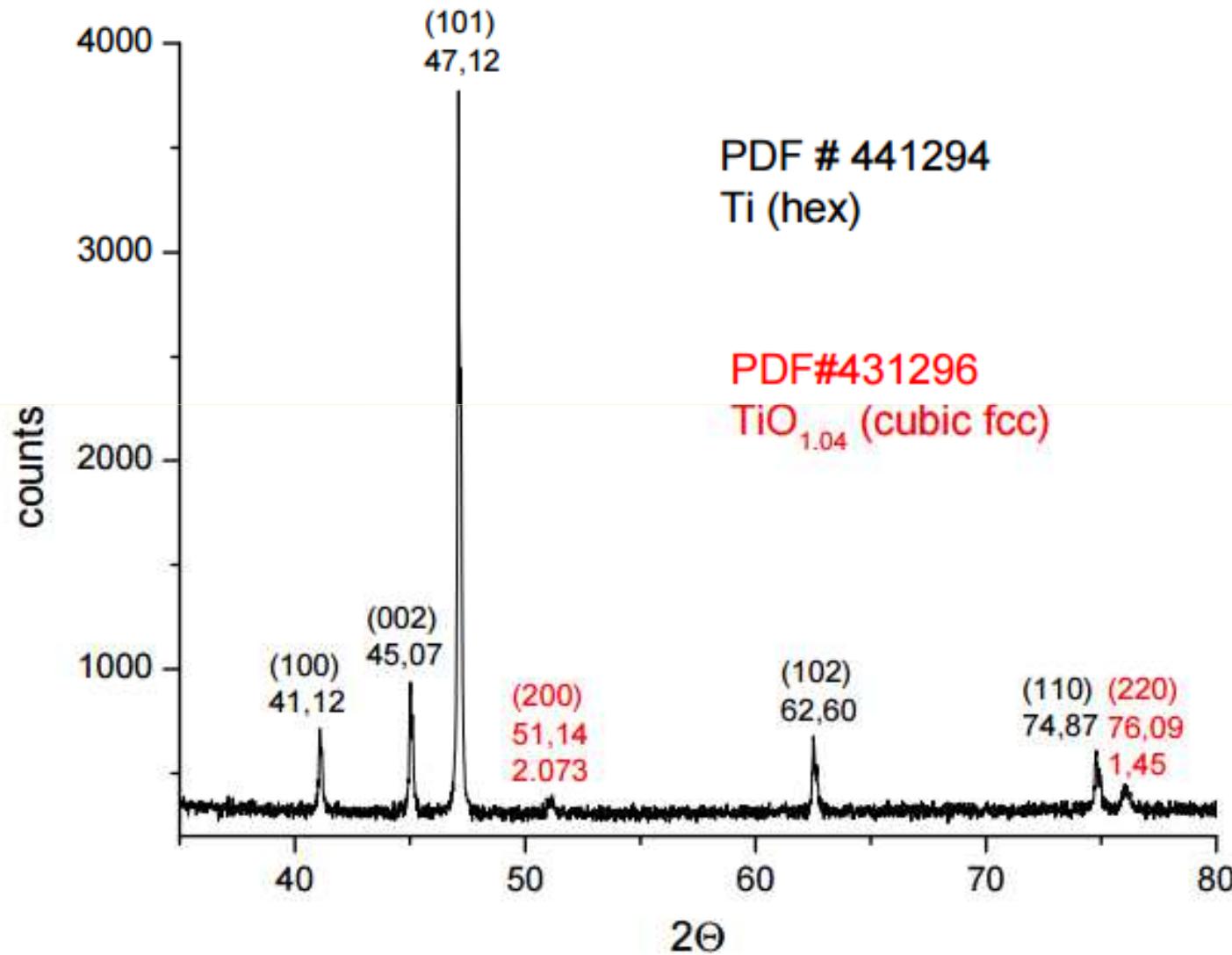
TITANIUM - XPS RESULTS



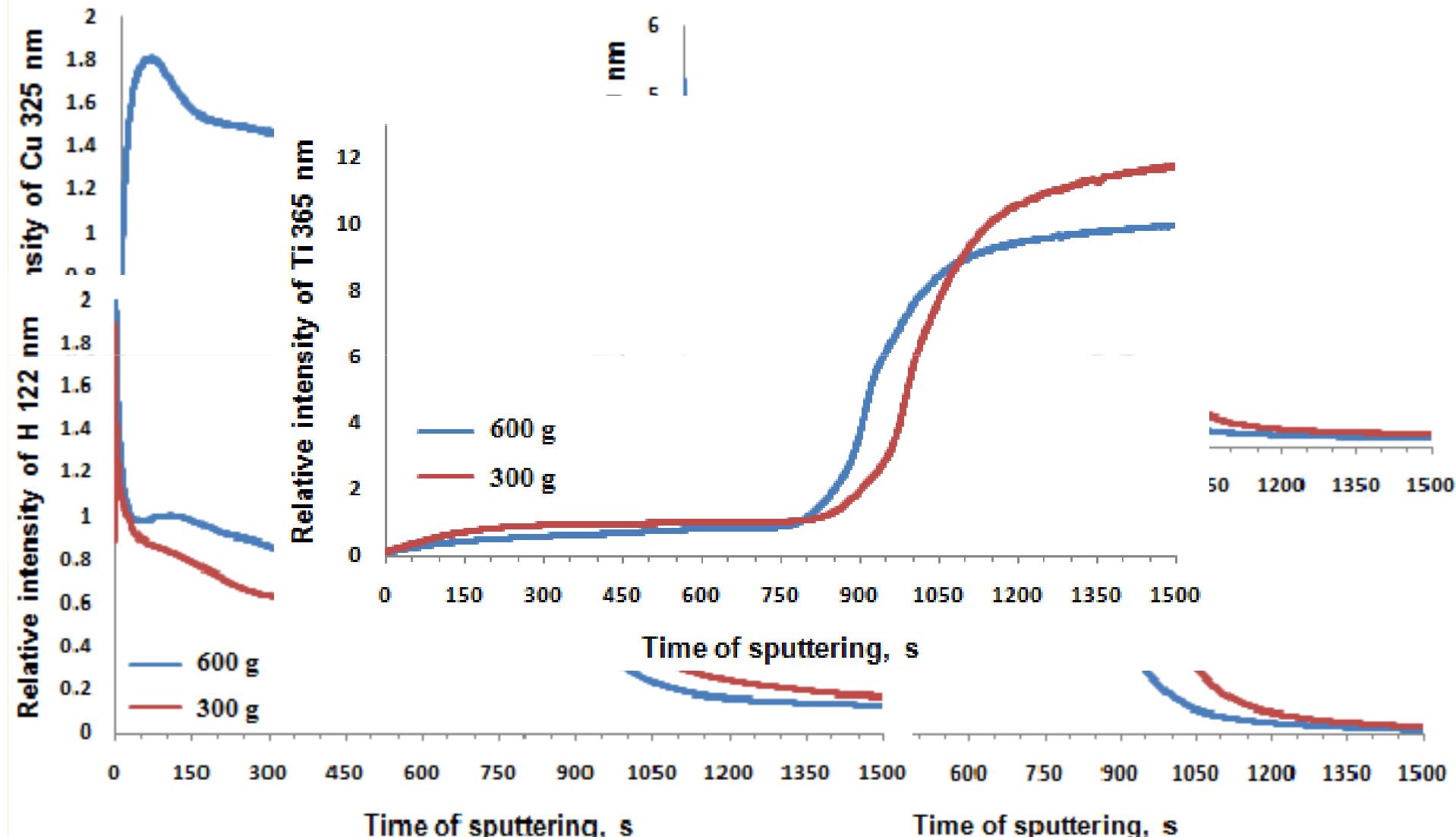
TITANIUM - XPS RESULTS



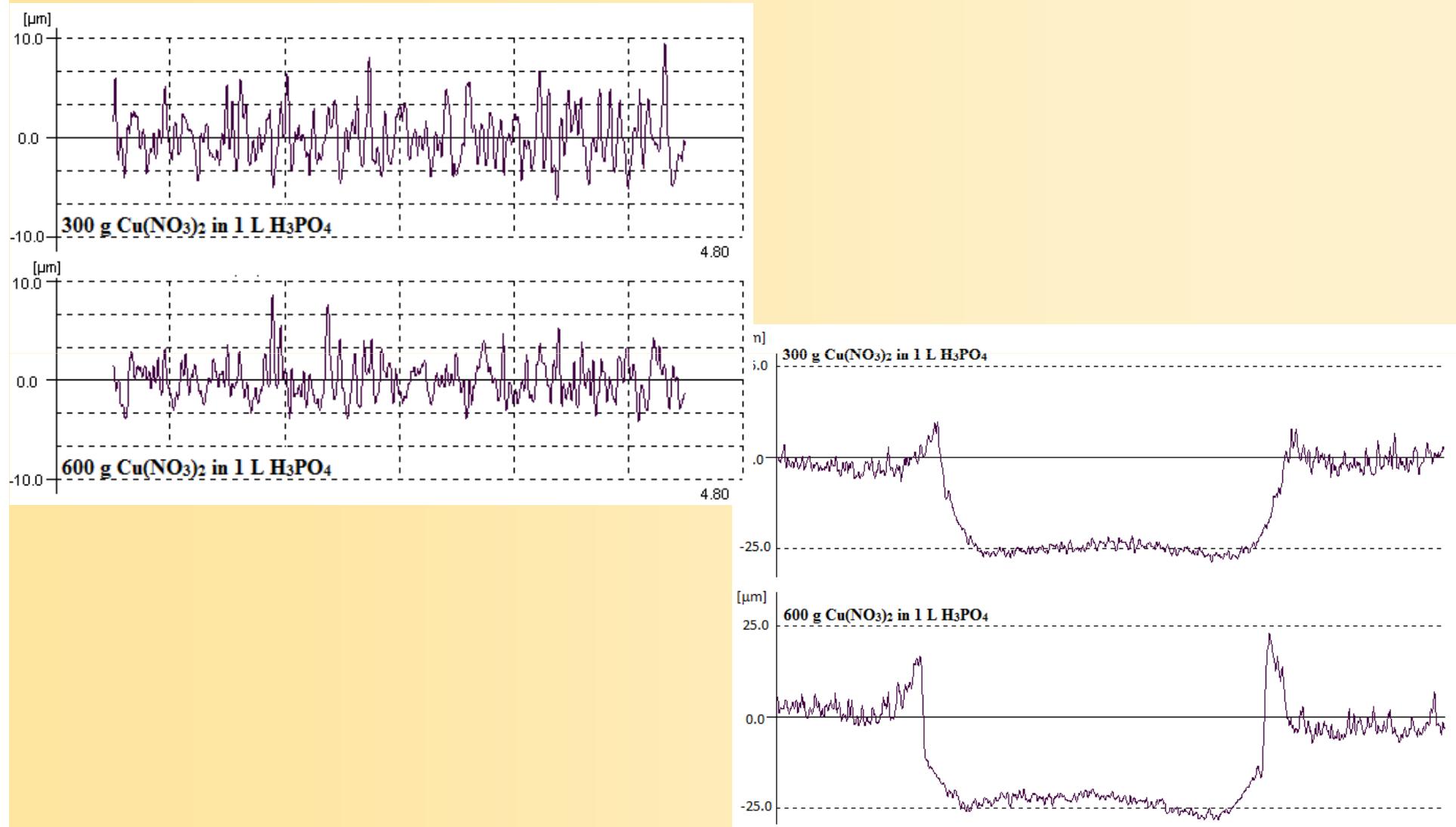
TITANIUM - XRD RESLTS



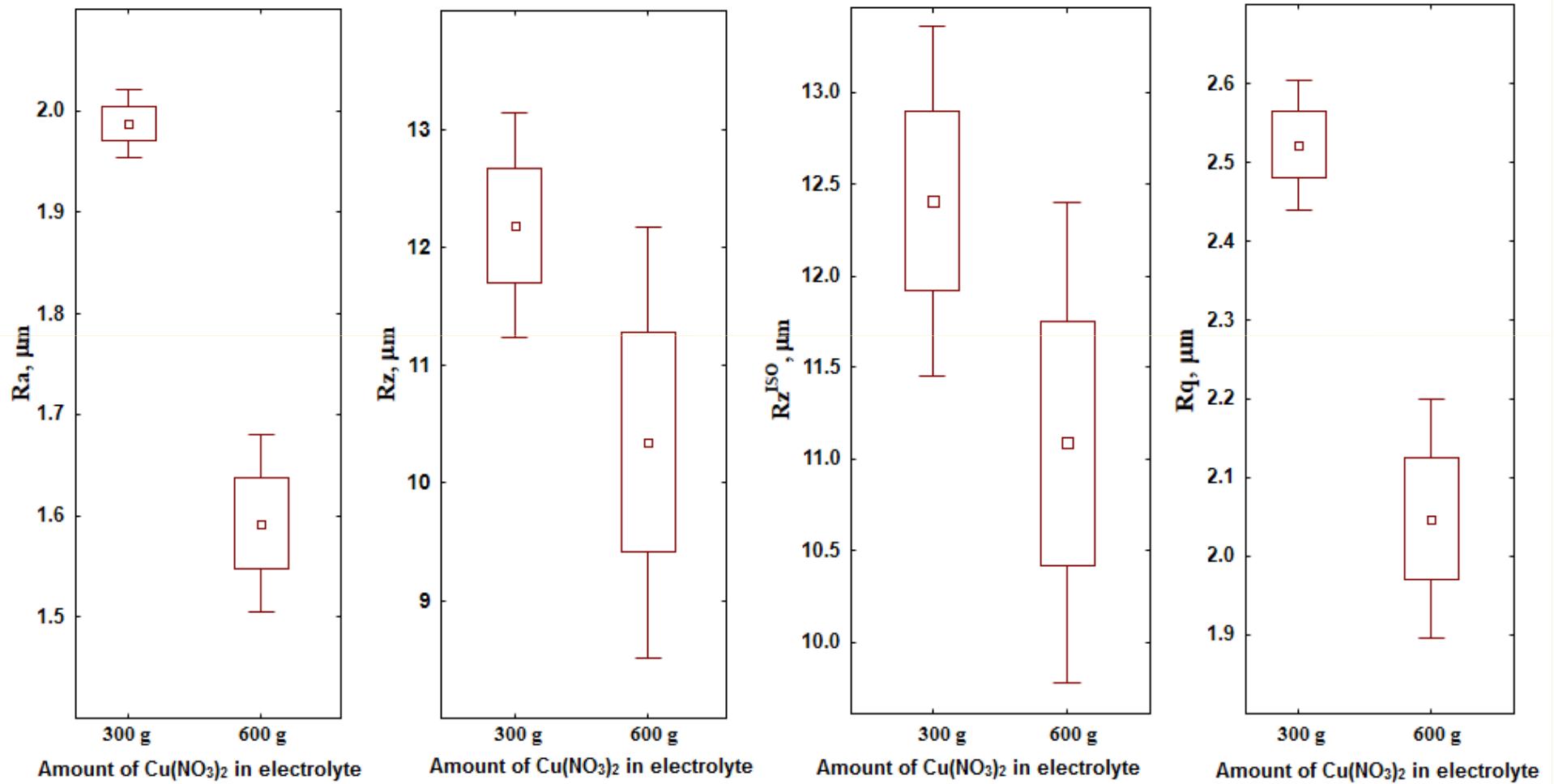
TITANIUM - GDOES RESULTS



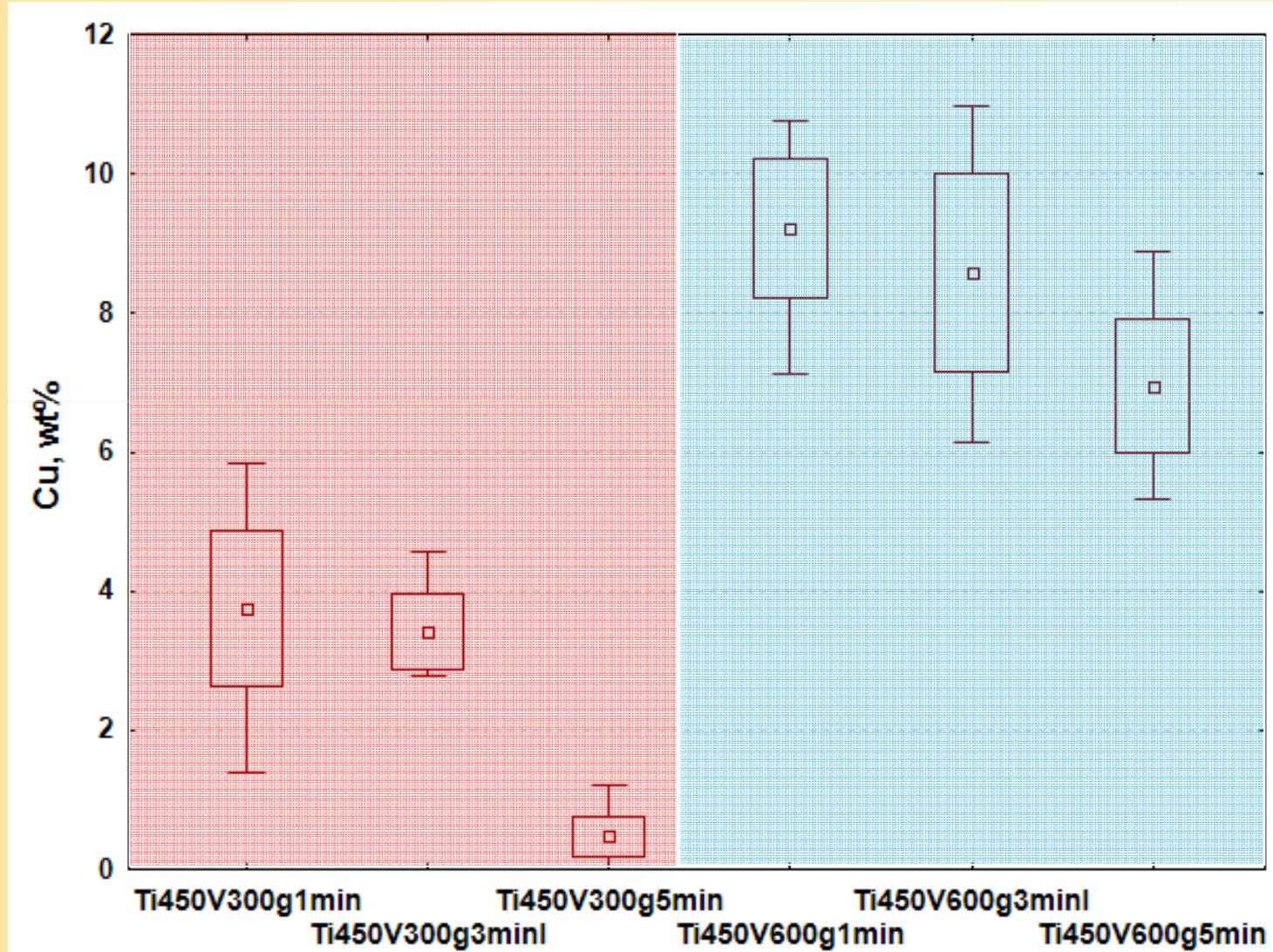
TITANIUM - 2D PROFILES



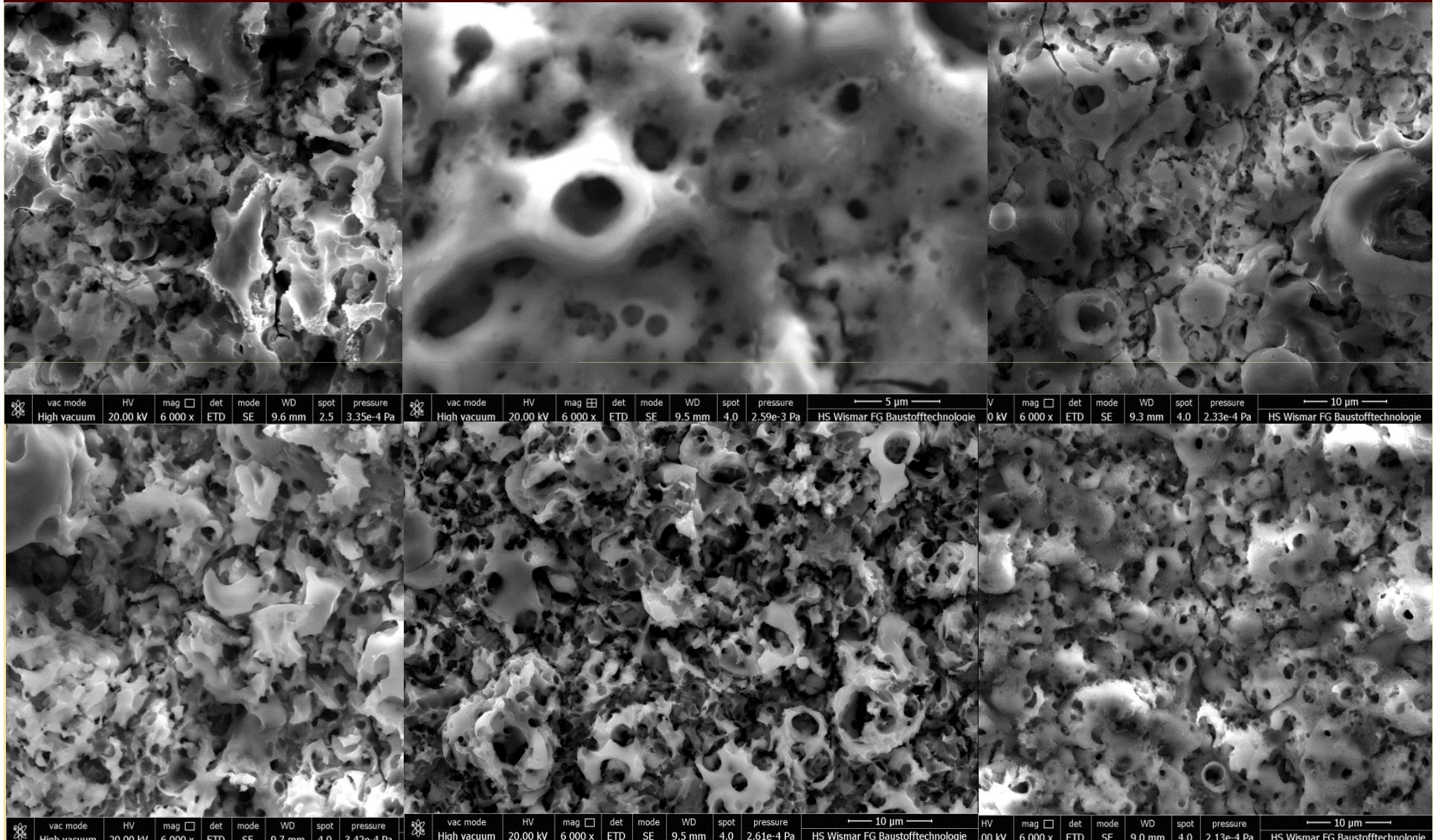
ROUGHNESS RESULTS



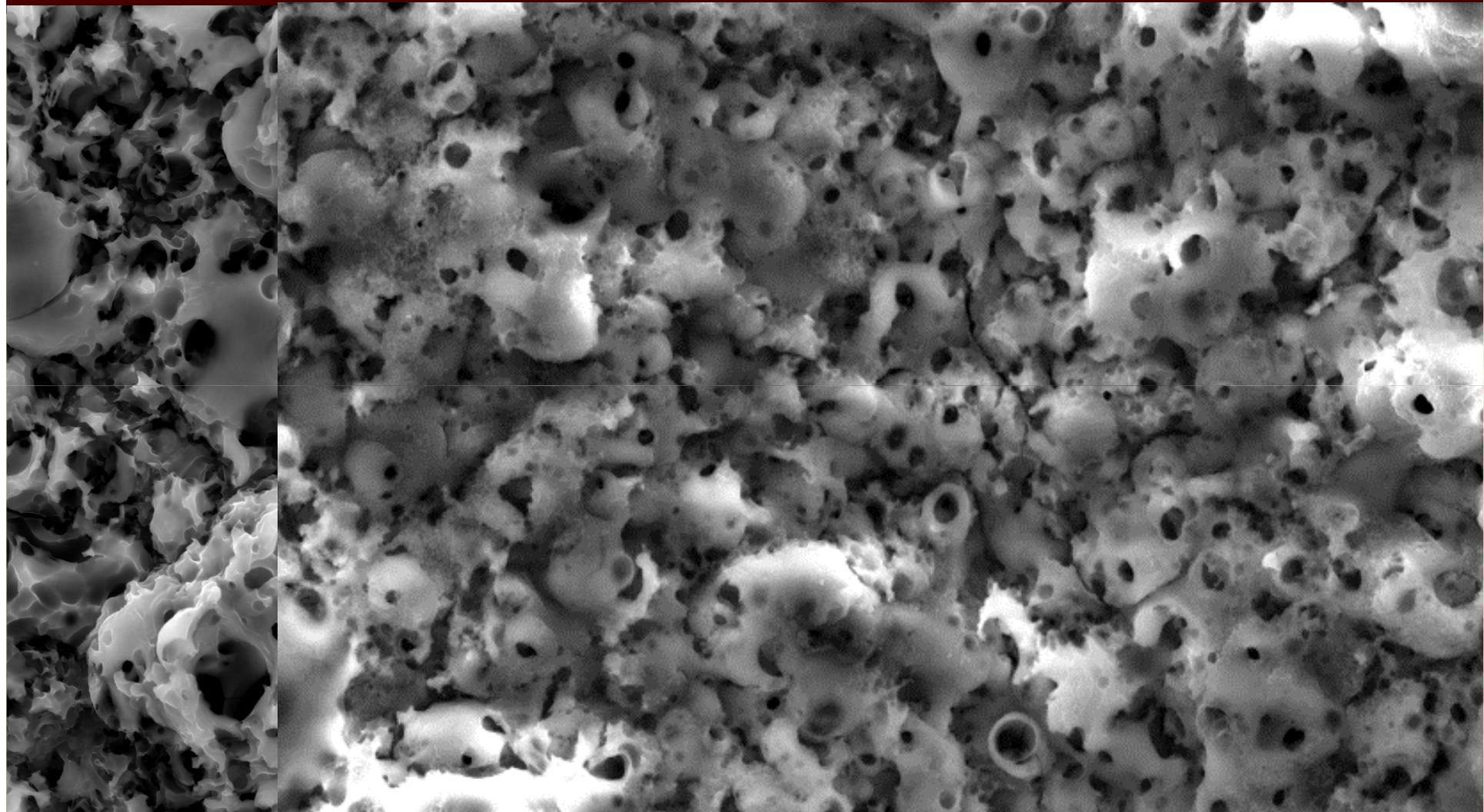
TITANIUM - RESULTS



SEM - RESULTS



TITANIUM SEM RESULTS



vac mode
High vacuum 20.00



vac mode
High vacuum



HV
20.00 kV



mag

6 000 x



det



mode



WD
9.0 mm



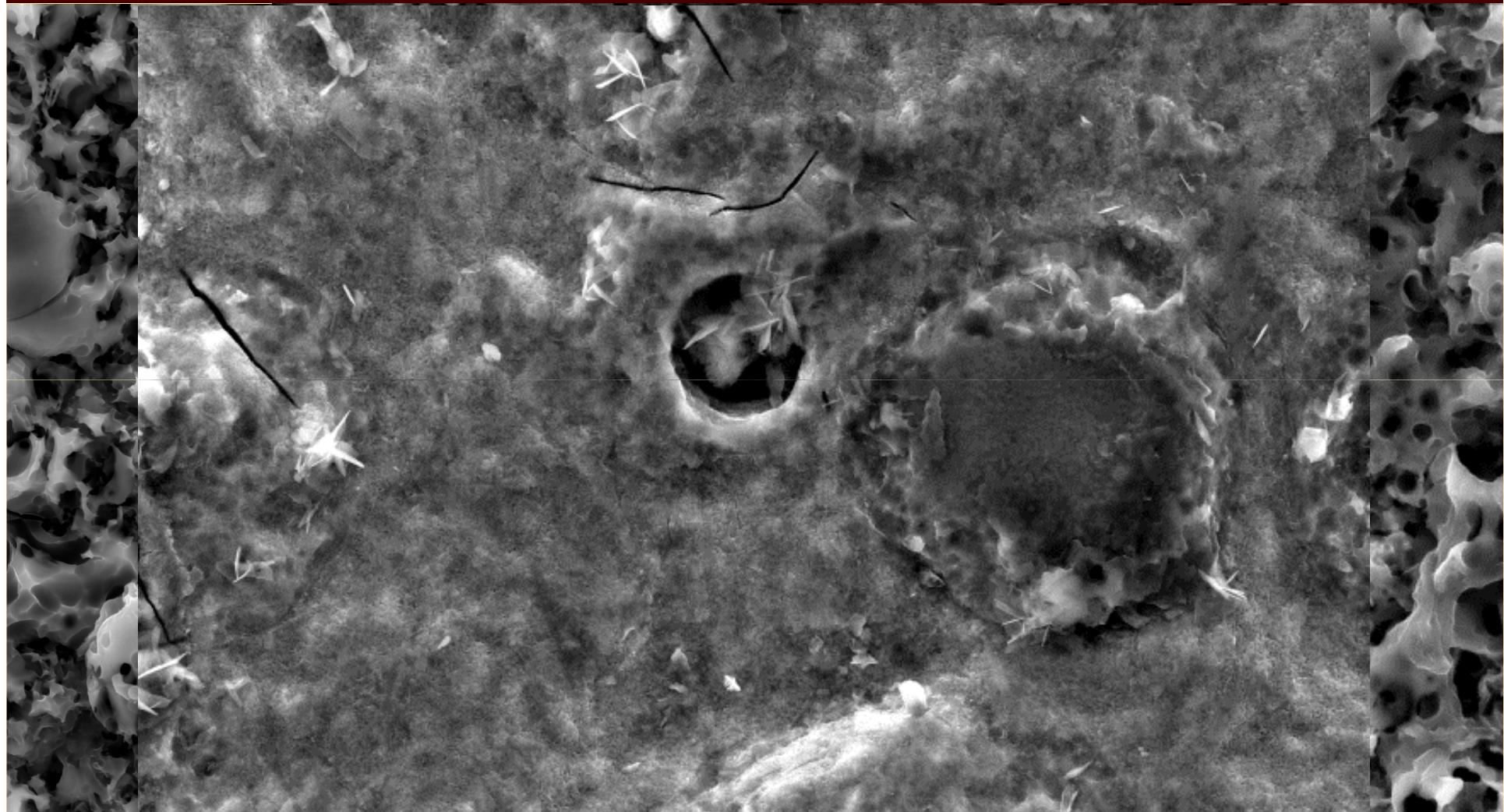
spot
4.0



pressure
2.13e-4 Pa

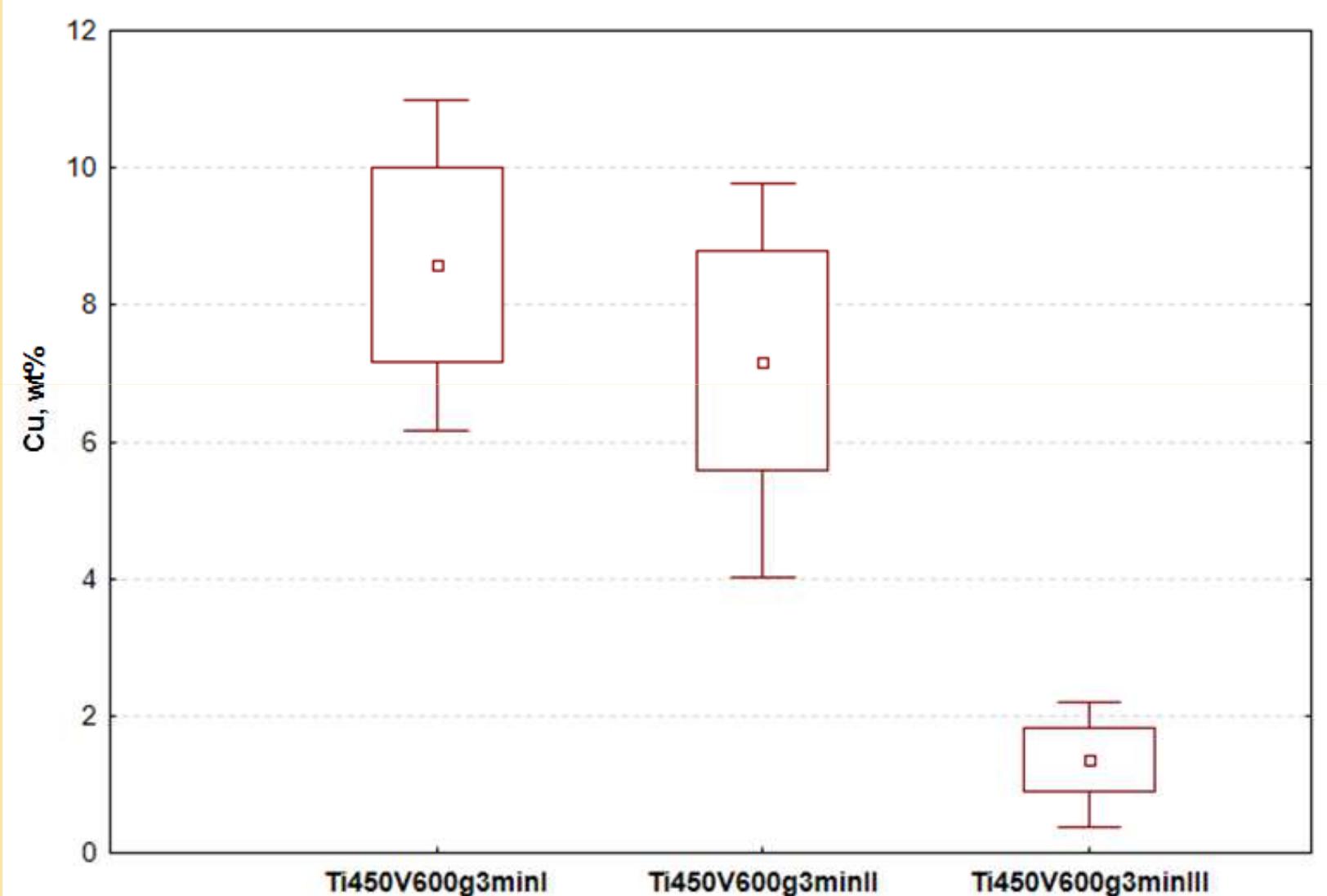
— 10 µm —
HS Wismar FG Baustofftechnologie

TITANIUM - SEM RESULTS

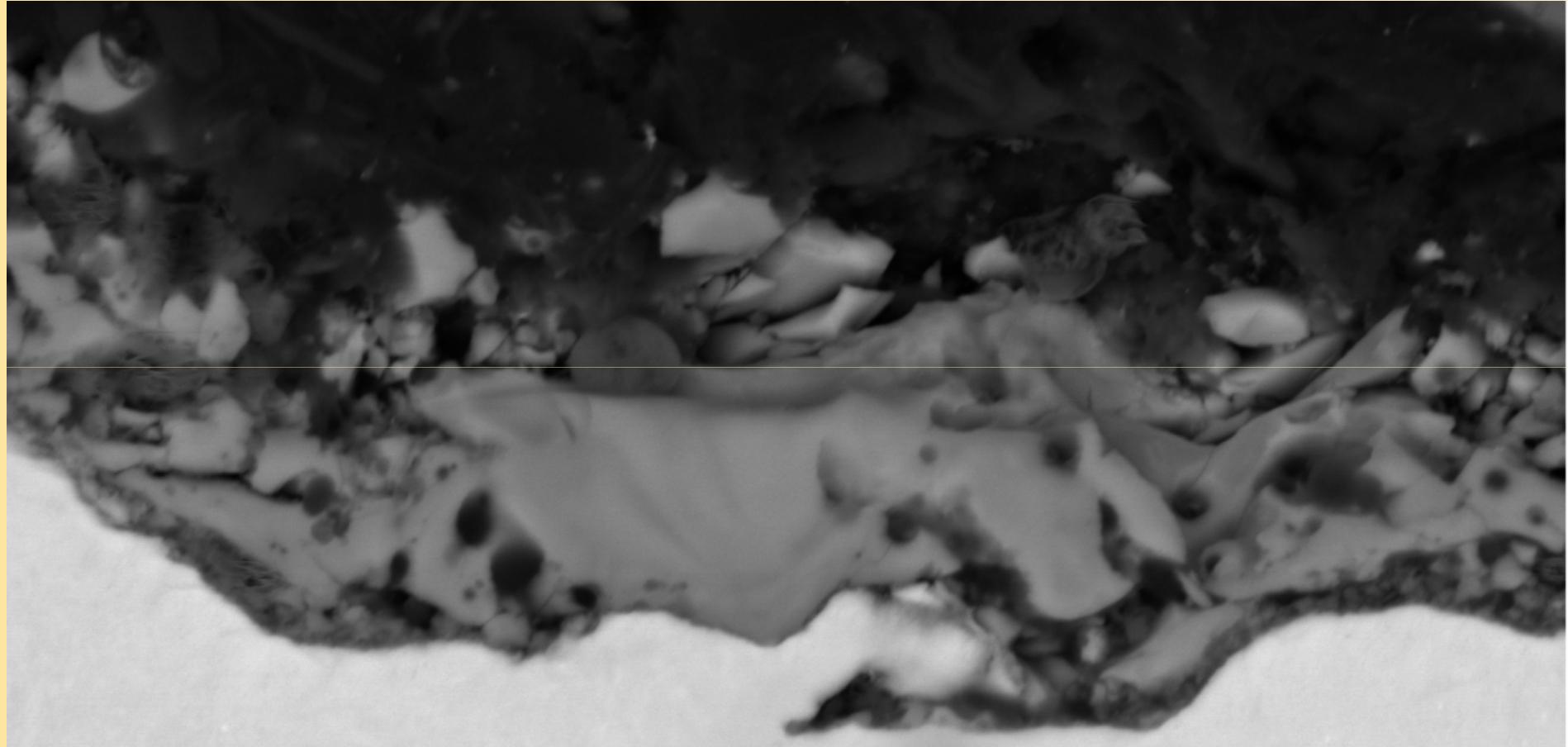


vac r	High v	vac mode	HV	mag	det	mode	WD	spot	pressure	— 10 µm —	→
		High vacuum	20.00 kV	6 000 x	ETD	SE	9.1 mm	4.0	3.20e-4 Pa	HS Wismar FG Baustofftechnologie	technologie

TITANIUM RESULTS

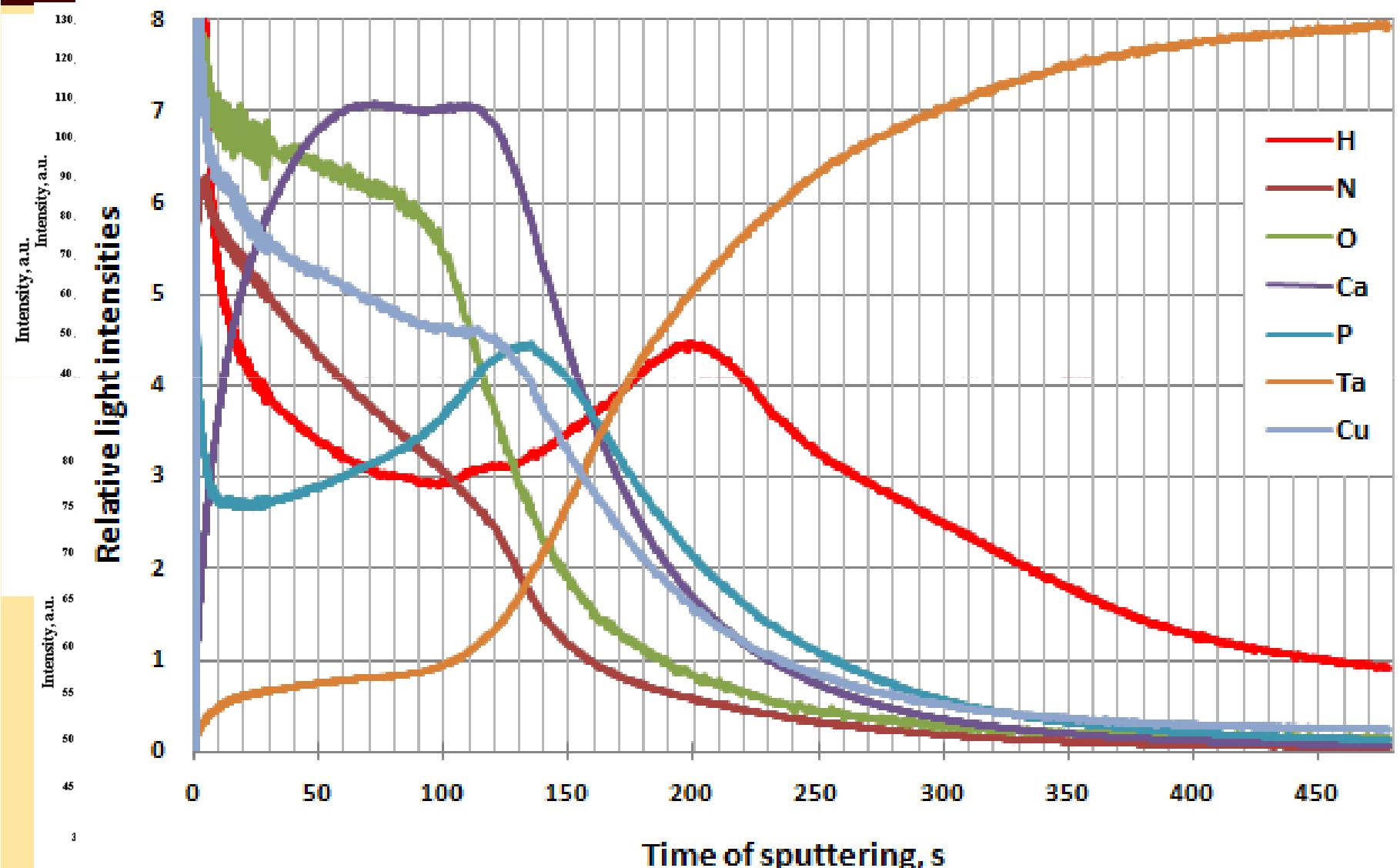


TITANIUM - SEM RESULTS



2/5/2015 9:03:14 AM	mag □ 6 000 x	WD 10.0 mm	HV 15.00 kV	spot 6.0	pressure 9.64e-4 Pa	det BSED	— 10 µm — Quanta 650 FEG
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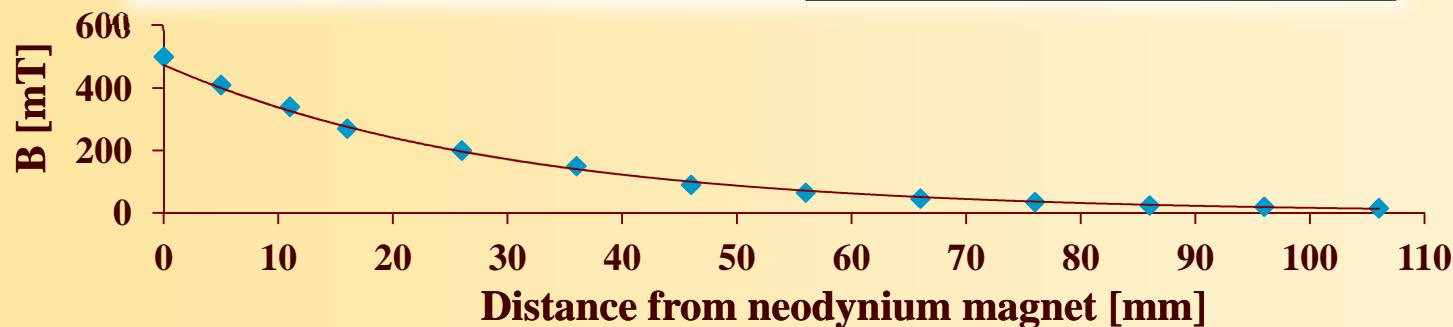
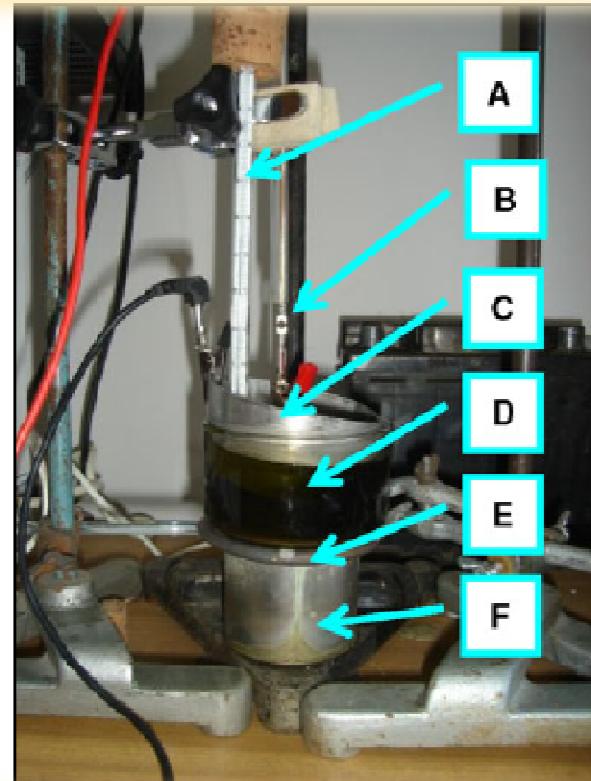
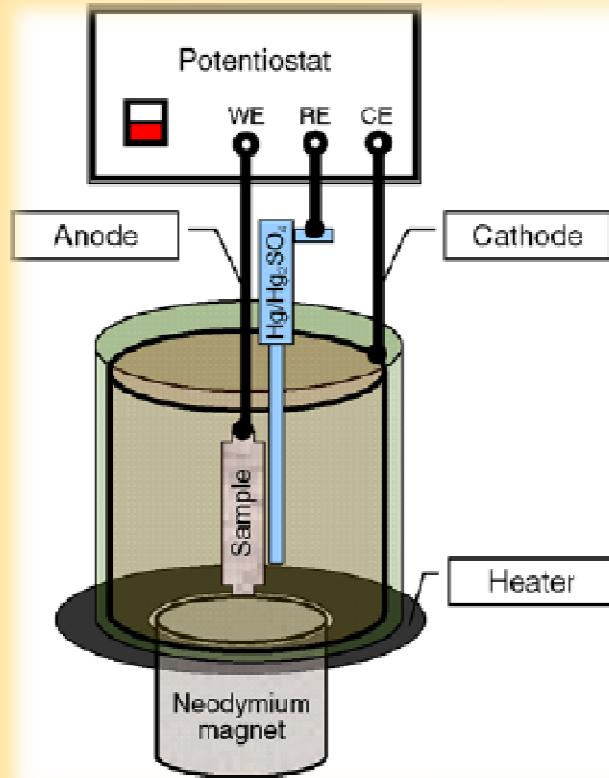
PEO ON TANTALUM



OTHER RESULTS

OTHER SCIENTIFIC INTERESTS

SET UP FOR MEP



ELECTROPOLISHING

SAMPLES

STEEL

Cylinder: $\phi = 10$ [mm], $h = 1$ [mm]
Cuboid: 5 X 30 X 1 [mm]



NITINOL dental drills



TITANIUM

Cylinder : $\phi = 0.8$ [mm], $h = 70$ [mm]
Cuboid : 10 x 2 x 50 [mm]



ELECTROLYTE

STEEL

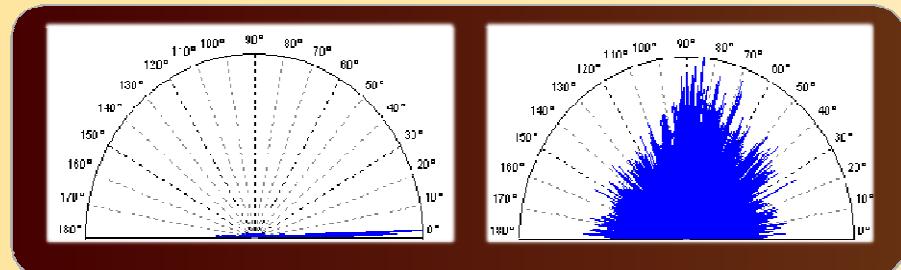
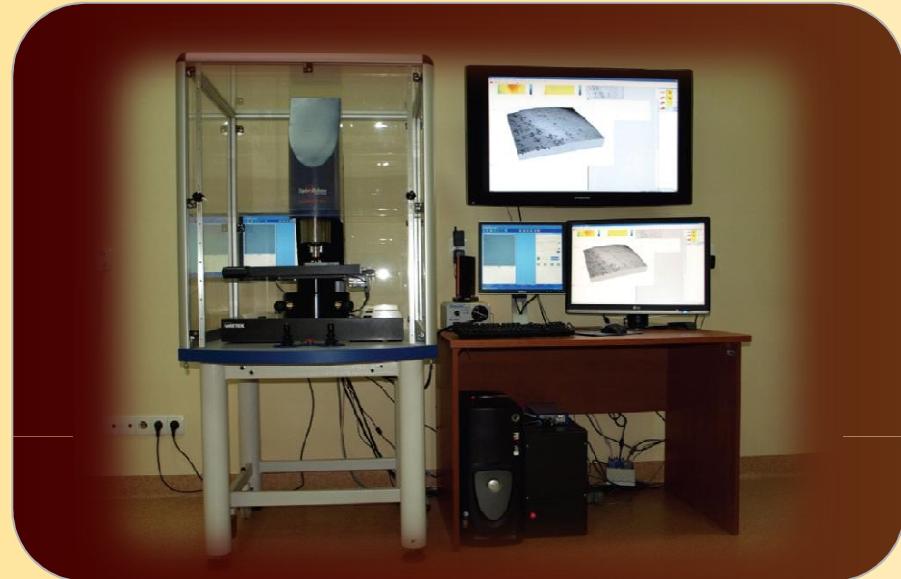
$\text{H}_2\text{SO}_4 : \text{H}_3\text{PO}_4 = 2 : 3$ (vol.)
10% of water in electrolyte (vol.)
Conductivity : 5,6 S/cm²
Temperature: $65 \pm 5^\circ\text{C}$
Density: 1,685 g/cm³
Viscosity : 215 mPa·s
 $\text{pH} = -1,15$

TITANIUM AND ITS ALLOYS

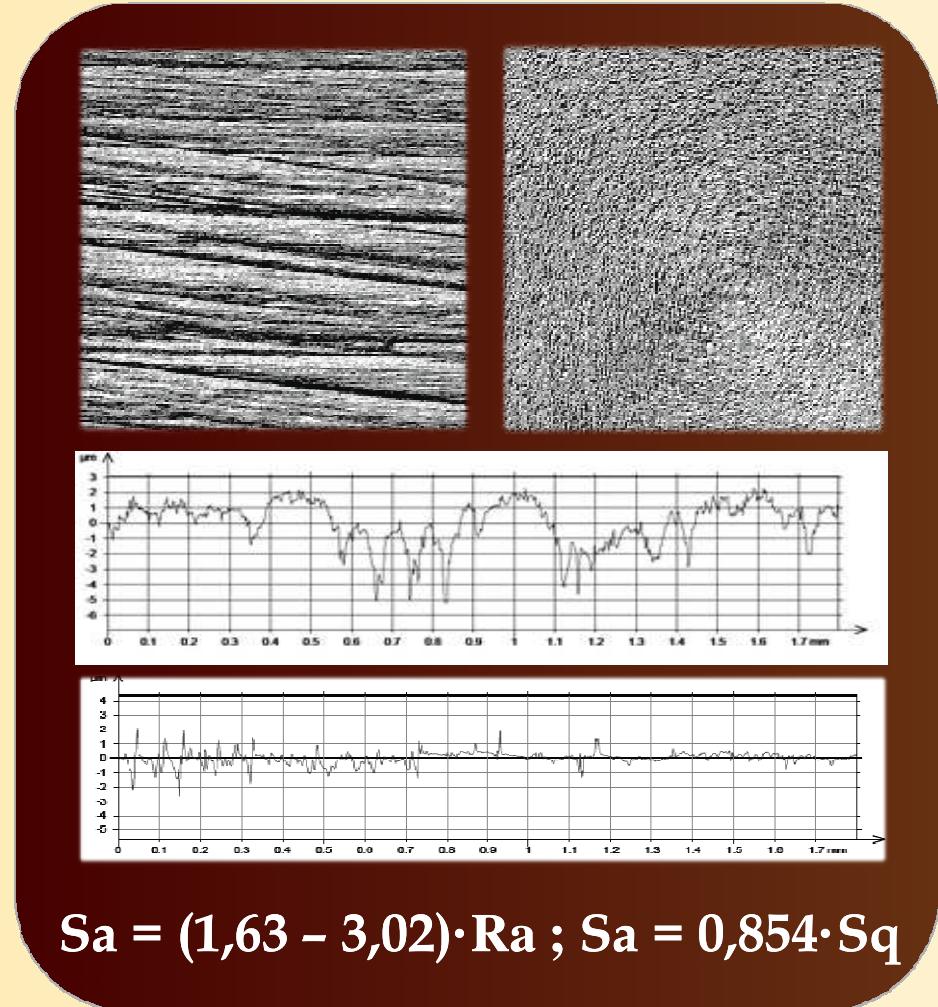
10 % H_2SO_4 + 5 % HF + 85% CH_3OH



ROUGHNESS OF THE SURFACES

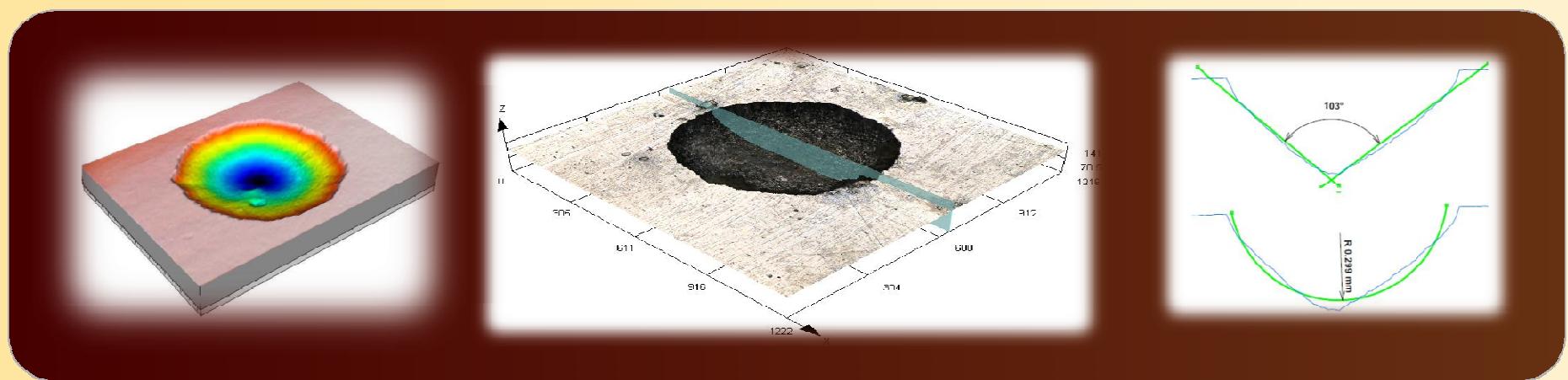
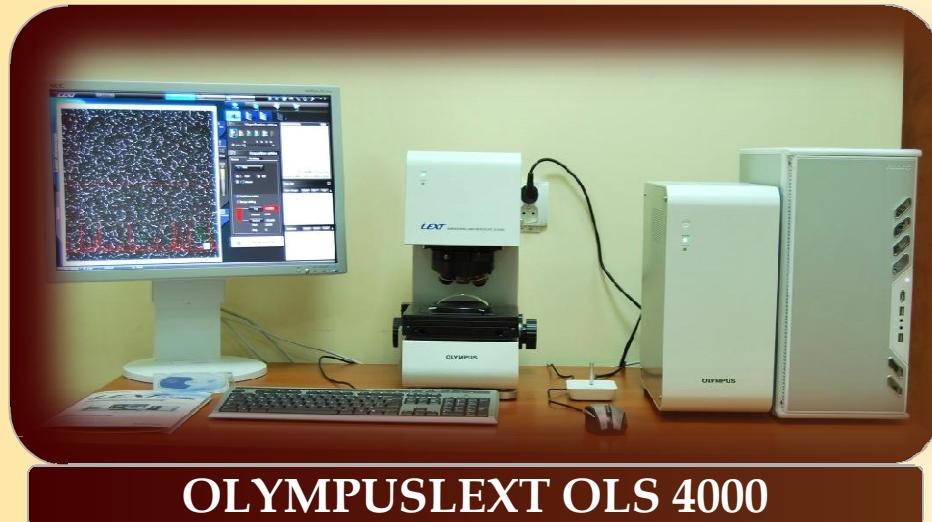


TALYSURF CCI 6000



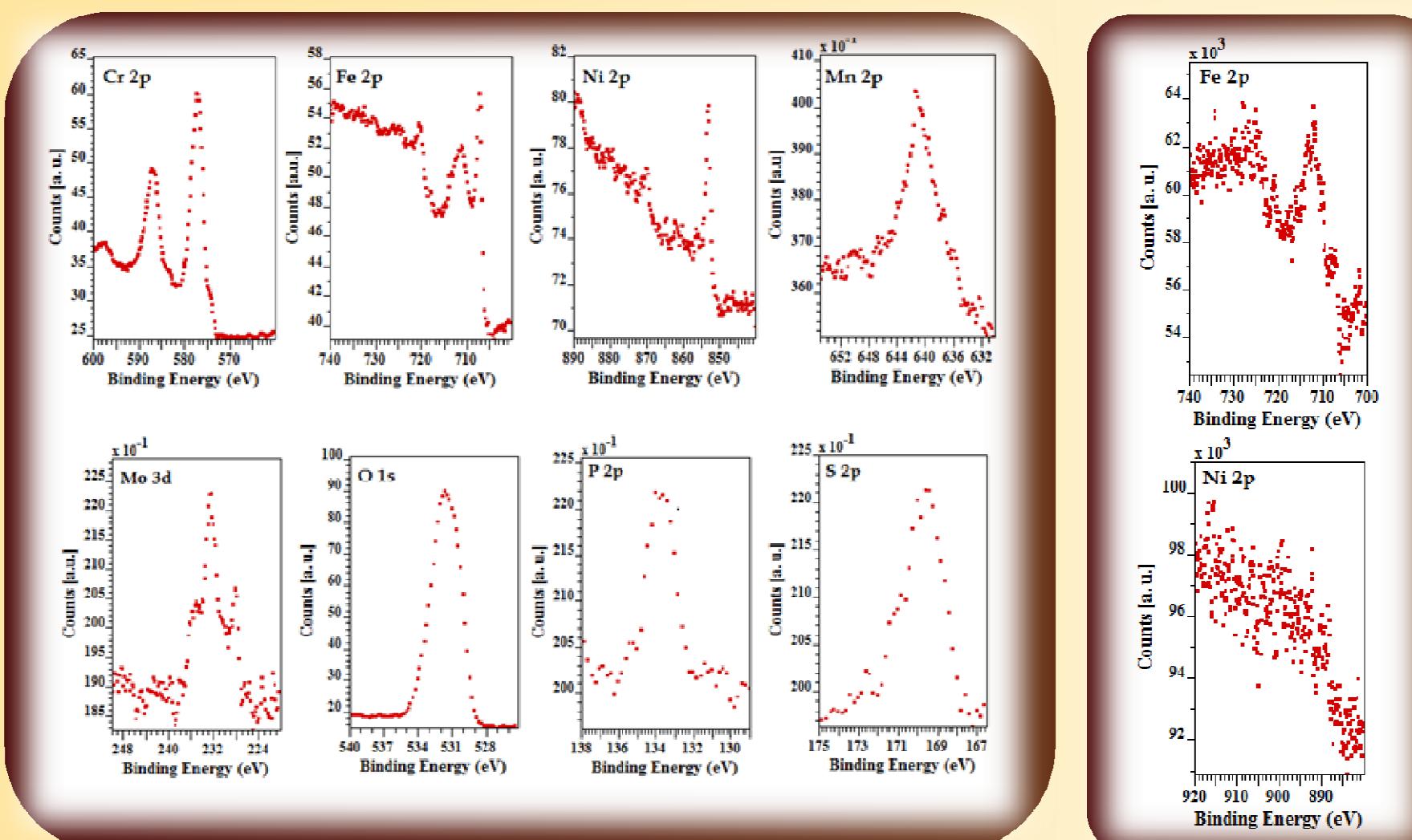
$$Sa = (1,63 - 3,02) \cdot Ra ; Sa = 0,854 \cdot Sq$$

PITS GEOMETRY

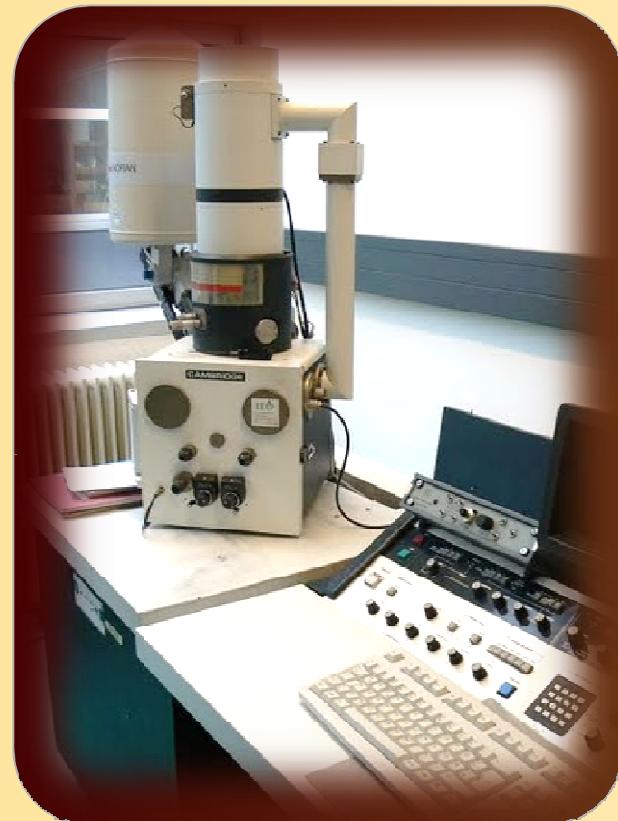


WYDZIAŁ MECHANICZNY - KATEDRA MECHANIKI PRECYZYJNEJ - LABORATORIUM MIKRO I NANOINŻYNIERII

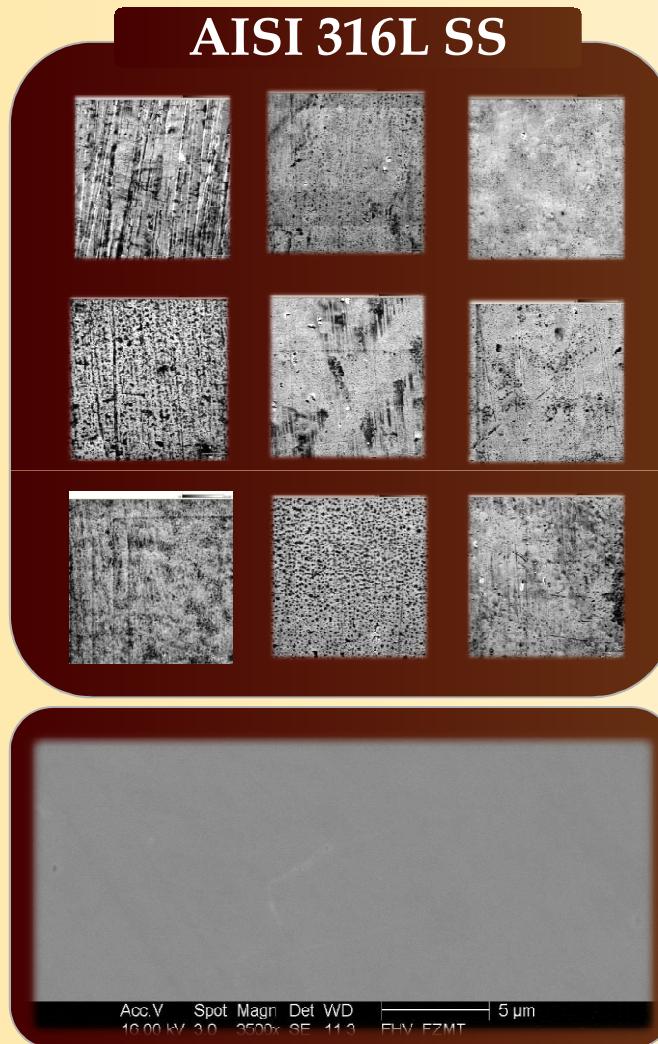
AISI 316L - XPS RESULTS



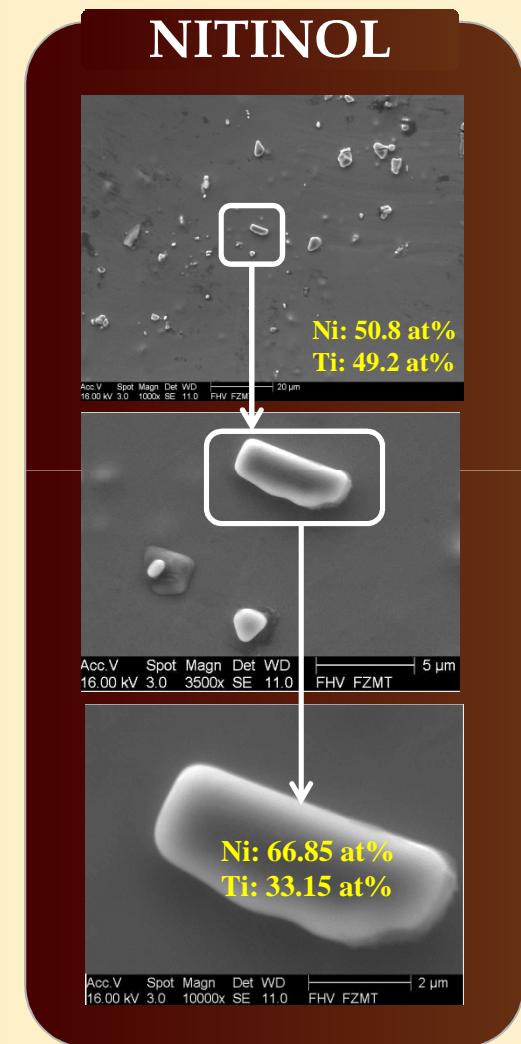
SEM/EDX



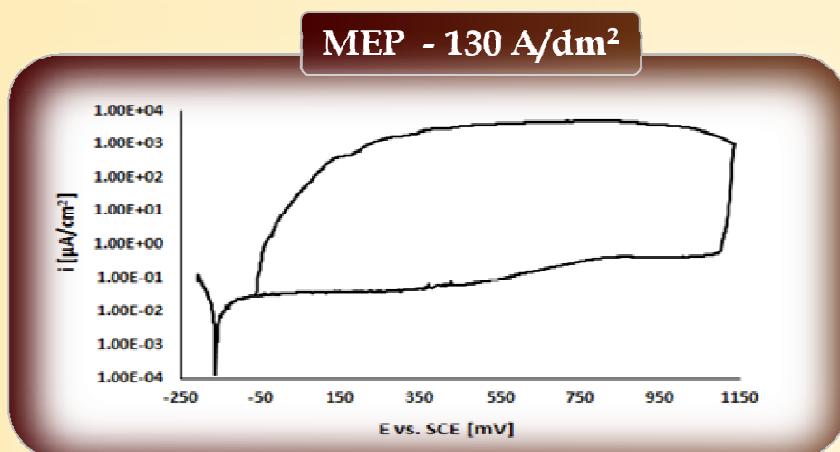
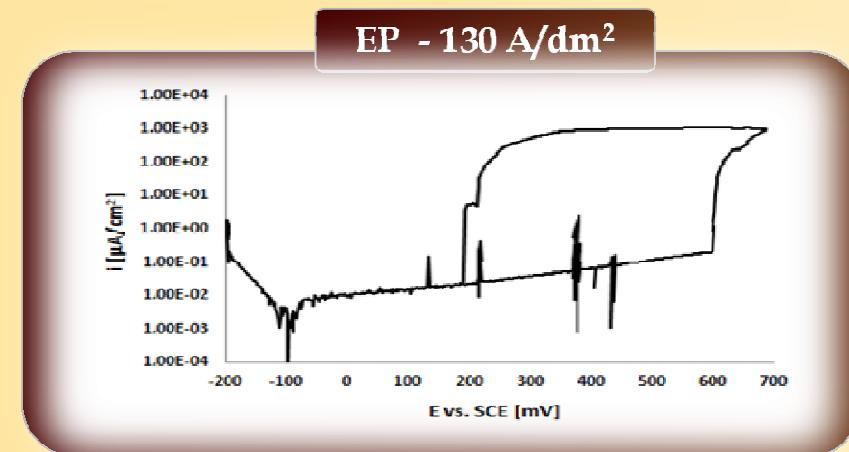
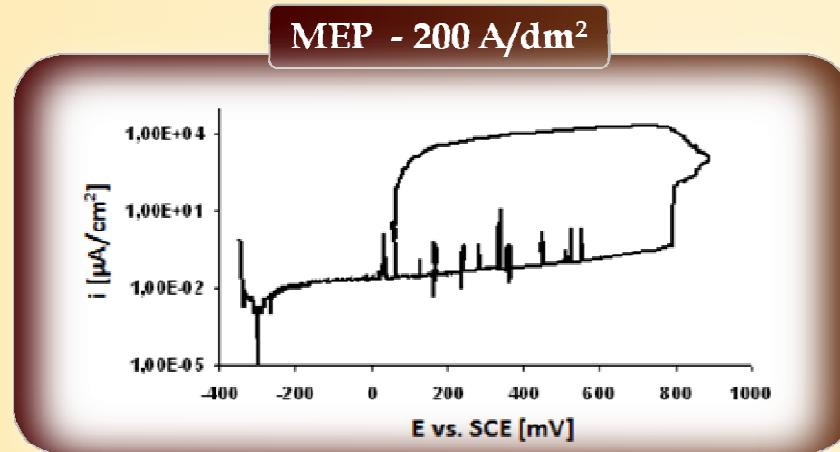
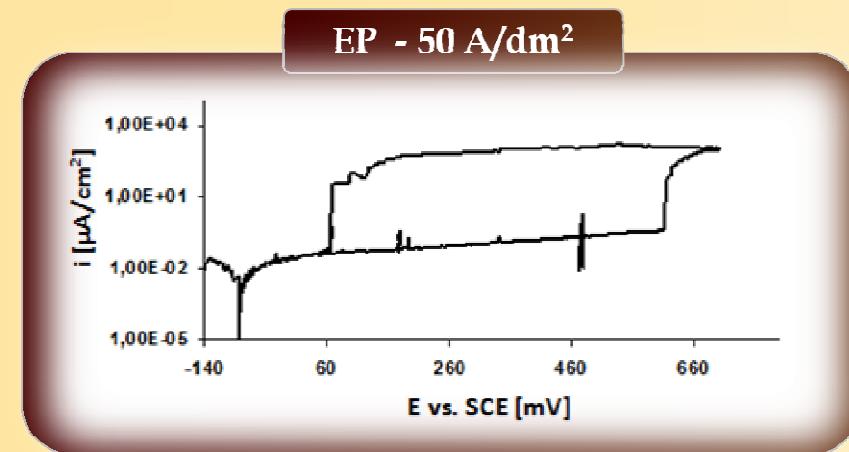
CAMBRIDGE S200



HOCHSCHULE NEUBRANDENBURG (GERMANY)



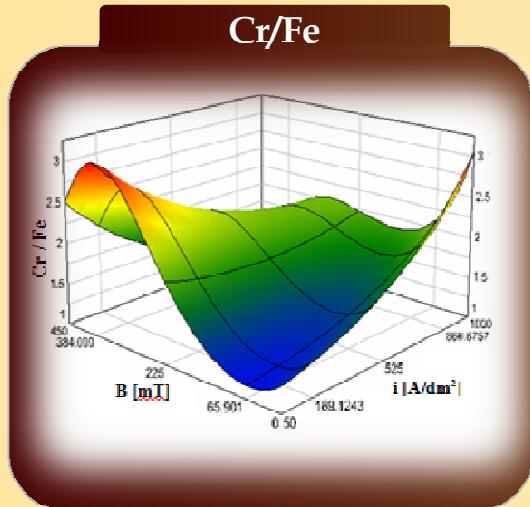
PITTING CORROSION – AISI 316L SS



Rokosz K., Hryniwicz T., Raaen S., Characterization of Passive Film Formed on AISI 316L Stainless Steel after Magnetoelectropolishing in a Broad Range of Polarization Parameters, Steel Research International, Vol. 83, Online ISSN: 1869-344X, 2012, 1-9.

SURFACE LAYERS AFTER MEP

Cr/Fe

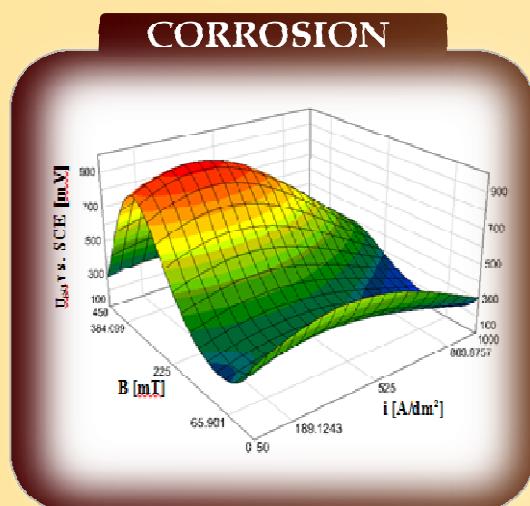


$$Epit(B, i) = \alpha(B, i) \pm 372,017 \cdot \sqrt{\beta(B, i)}$$

$$0 \quad mT \leq B \leq 450 \quad mT$$

$$50 \quad \frac{A}{dm^2} \leq i \leq 1000 \quad \frac{A}{dm^2}$$

CORROSION

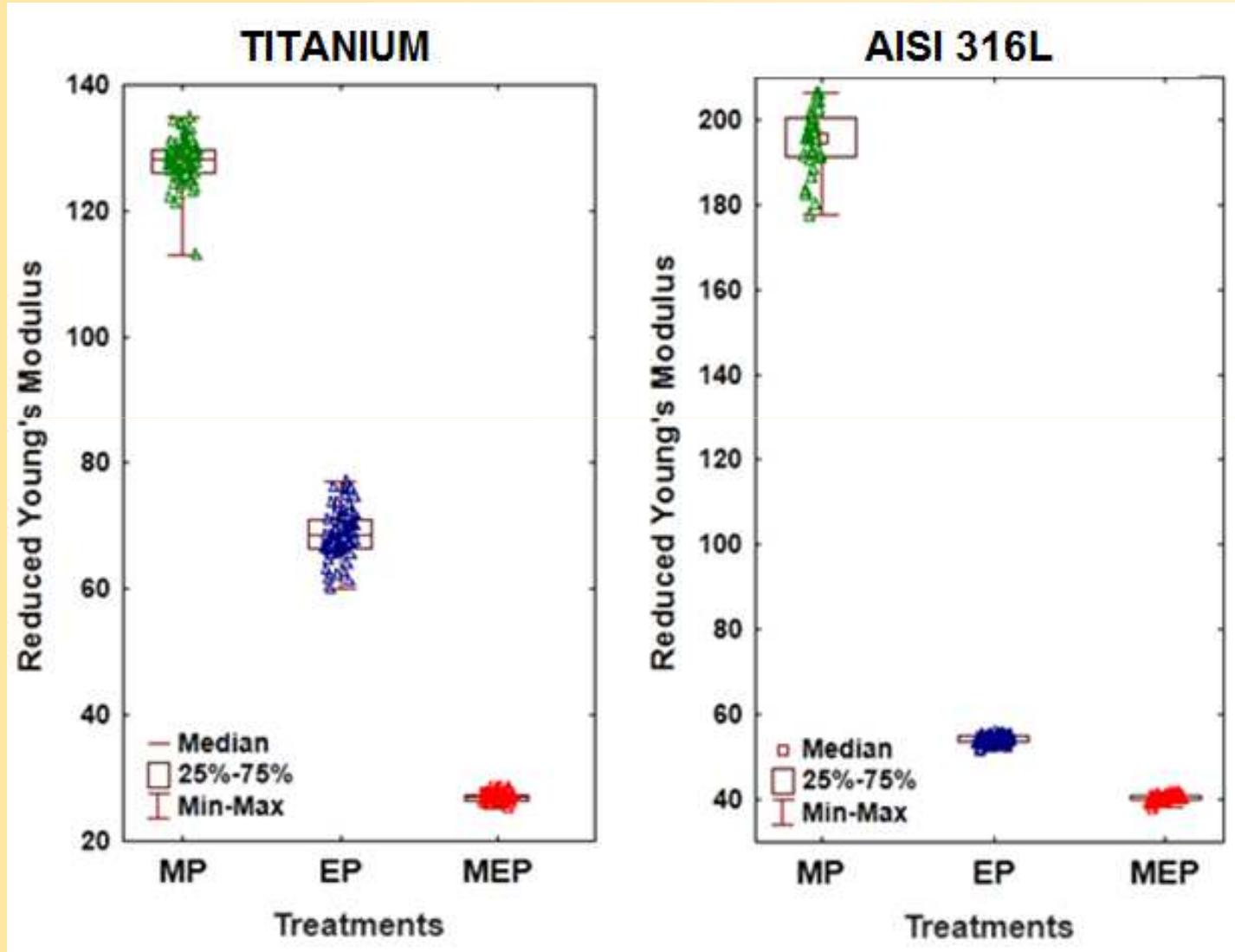


$$\alpha(B, i) = 4717 - 3,96 \cdot B - 6,178 \cdot i - \frac{417}{10^5} B \cdot i + \frac{2}{10^3} B^2 - \frac{228}{10^5} i^2 - \frac{349}{10^{11}} B^2 i^2 - \frac{7,9 \cdot 10^{-5}}{B + i}$$

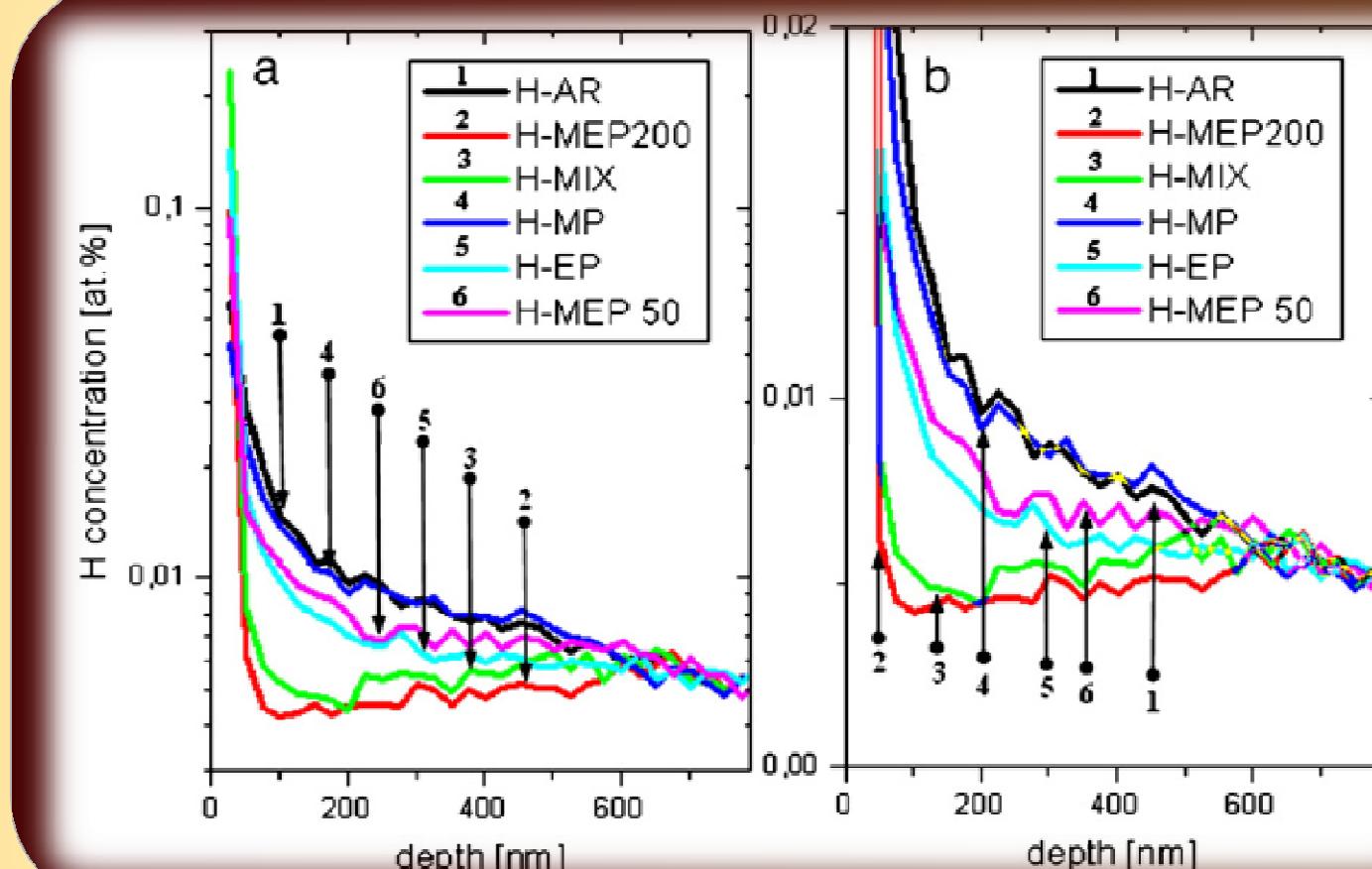
$$\begin{aligned} \beta(B, i) = & 54,5 - 0,218 \cdot B - 18,5 \cdot 10^{-2} \cdot i + 6,58 \cdot 10^{-4} \cdot B \cdot i + 3,94 \cdot 10^{-4} \cdot B^2 + 2,47 \cdot 10^{-4} \cdot i^2 + \\ & - 3,49 \cdot 10^{-10} \cdot (B \cdot i)^2 - 9 \cdot 10^{-7} \cdot B^2 \cdot i - 6,71 \cdot 10^{-7} \cdot B \cdot i^2 - 4,08 \cdot 10^{-7} \cdot B^3 - 15,36 \cdot \\ & \cdot 10^{-8} \cdot i^3 + 2,29 \cdot 10^{-10} \cdot B^4 + 3,84 \cdot 10^{-11} \cdot i^4 + 2,26 \cdot 10^{-10} \cdot B \cdot i^3 + 4,76 \cdot 10^{-13} \cdot B^2 \cdot \\ & \cdot i^3 - 2,34 \cdot 10^{-16} \cdot B^2 \cdot i^4 + 4,58 \cdot 10^{-10} \cdot B^3 \cdot i + 7,02 \cdot 10^{-13} \cdot B^3 \cdot i^2 - 11,08 \cdot 10^{-16} \cdot B^3 \\ & \cdot i^3 - 6,22 \cdot 10^{-16} \cdot B^4 \cdot i^2 + 8,57 \cdot 10^{-22} \cdot (B \cdot i)^4 - \frac{17060}{B + i} + \frac{32,4 \cdot B}{B + i} + \frac{28,4 \cdot i}{B + i} - 4,02 \cdot 10^{-2} \cdot \\ & \cdot \frac{B \cdot i}{B + i} - 18,42 \cdot 10^{-3} \cdot \frac{B^2}{B + i} - 13,02 \cdot 10^{-3} \cdot \frac{i^2}{B + i} + 34 \cdot 10^{-8} \cdot \frac{3(B \cdot i)^2}{B + i} + 137 \cdot 10^4 \frac{1}{(B + i)^2} \end{aligned}$$

ROKOSZ K., POLEROWANIE ELEKTROCHEMICZNE STALI W POLU MAGNETYCZNYM, WYD. UCZ. POLITECHNIKI KOSZALIŃSKIEJ, KOSZALIN 2012.

NANOINDENTATION



HYDROGENATION – AISI 316L SS

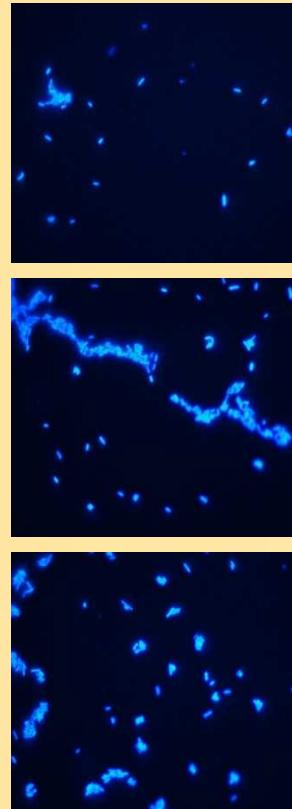


INSTYTUT TELE-I RADIOTECHNICZNY, LABORATORIUM BADAWCZO-POMIAROWE TECHNIKI PRÓŻNI

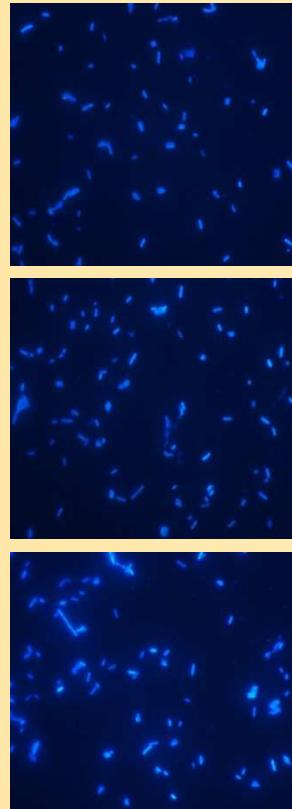
HYRNIEWICZ T., KONARSKI P., ROKOSZ K., ROKICKI R., SIMS ANALYSIS OF HYDROGEN CONTENT IN NEAR SURFACE LAYERS OF AISI 316L SS AFTER ELECTROLYTIC POLISHING UNDER DIFFERENT CONDITIONS, SURFACE & COATINGS TECHNOLOGY, 2011, 205, 4228-4236.

BIOLOGICAL STUDIES – AISI 316L

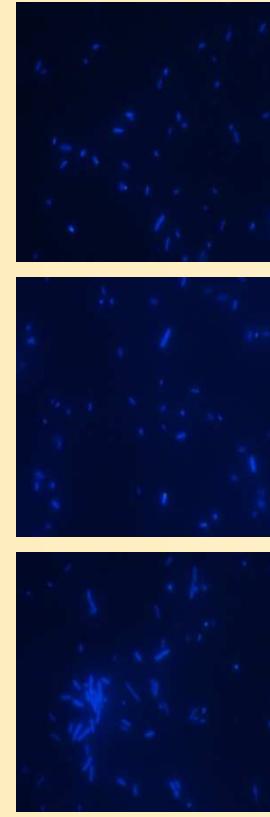
EP (2 h)



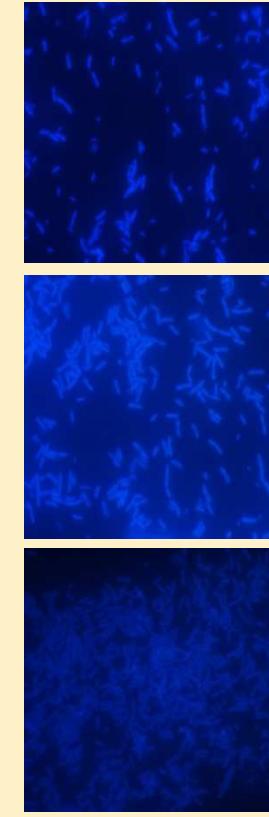
MEP (2h)



EP (4h)

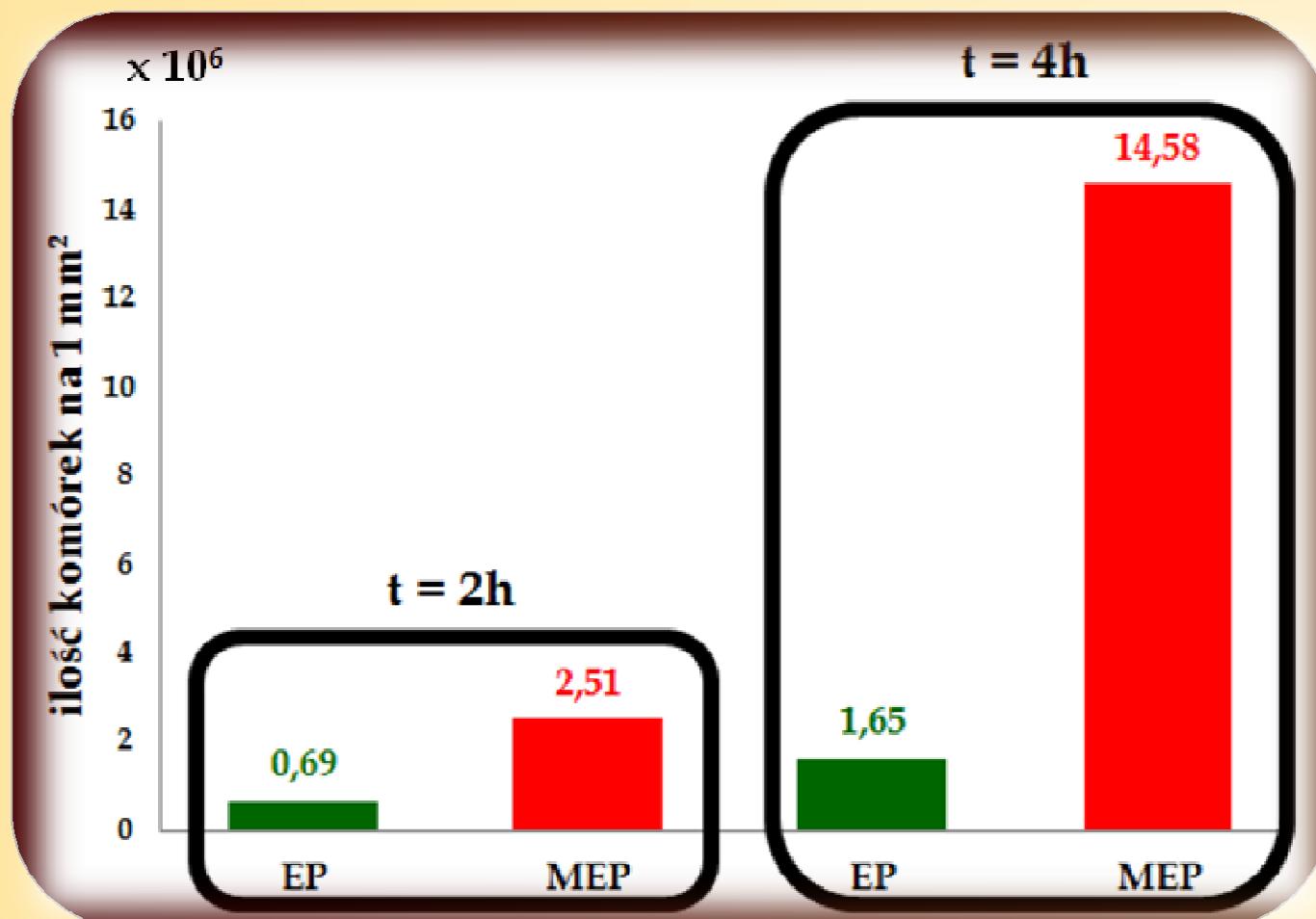


MEP (4h)

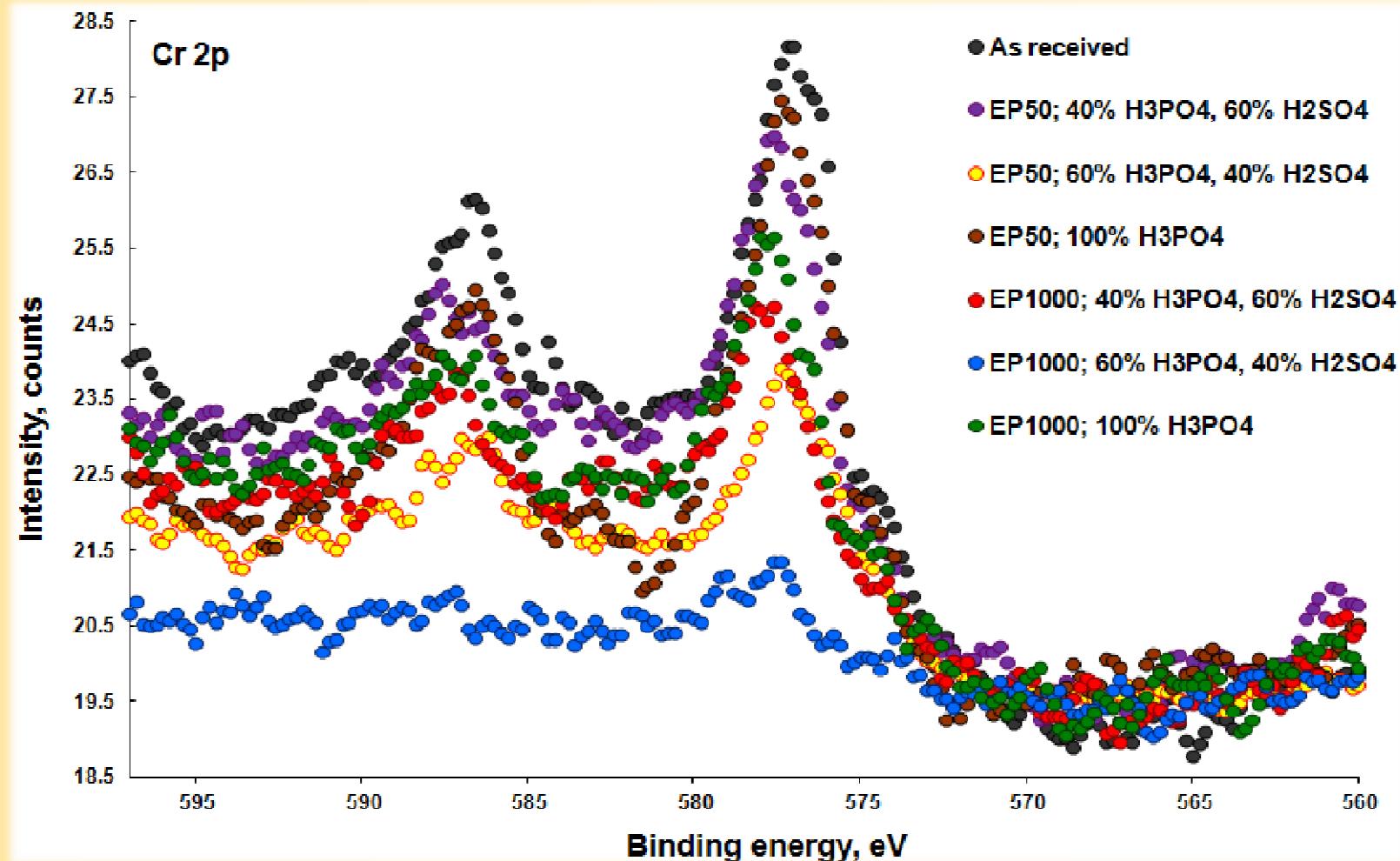


WYDZIAŁ INŻYNIERII ŁĄDOWEJ, ŚRODOWISKA I GEODEZJI - KATEDRA BIOLOGII ŚRODOWISKOWEJ

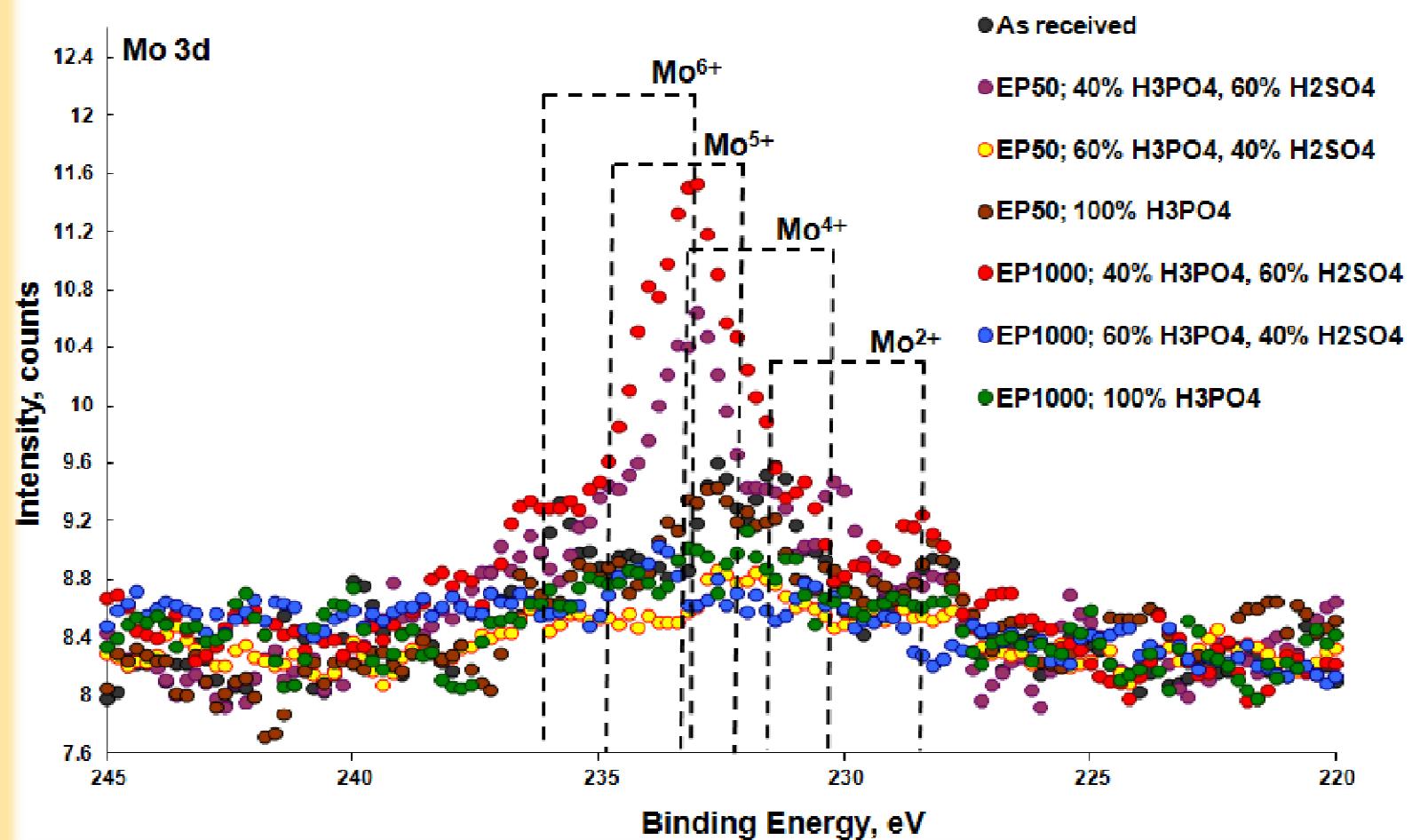
BIOLOGICAL STUDIES – AISI 316L



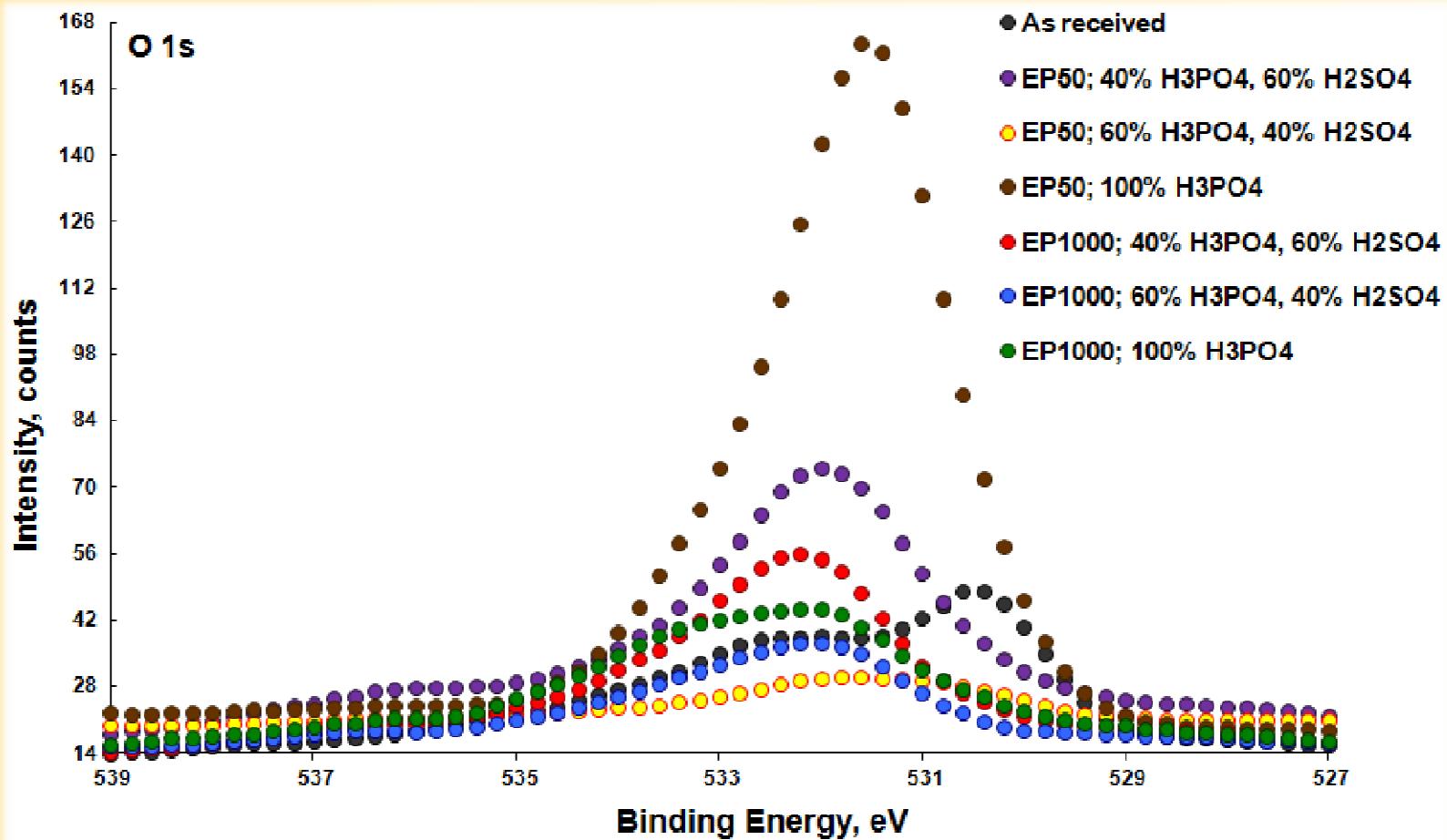
HIGH-CURRENT DENSITY ELECTROPOOLISHING



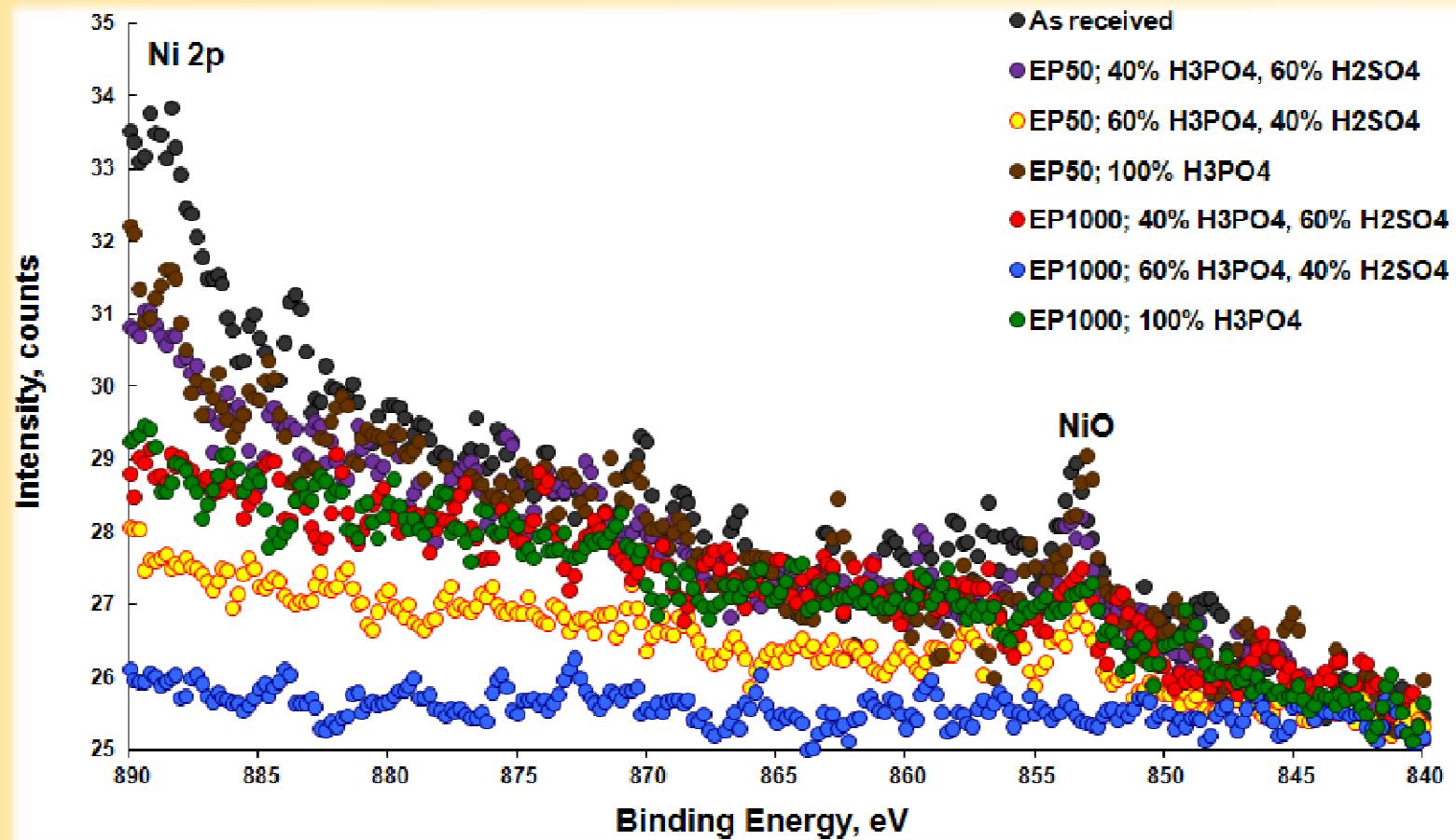
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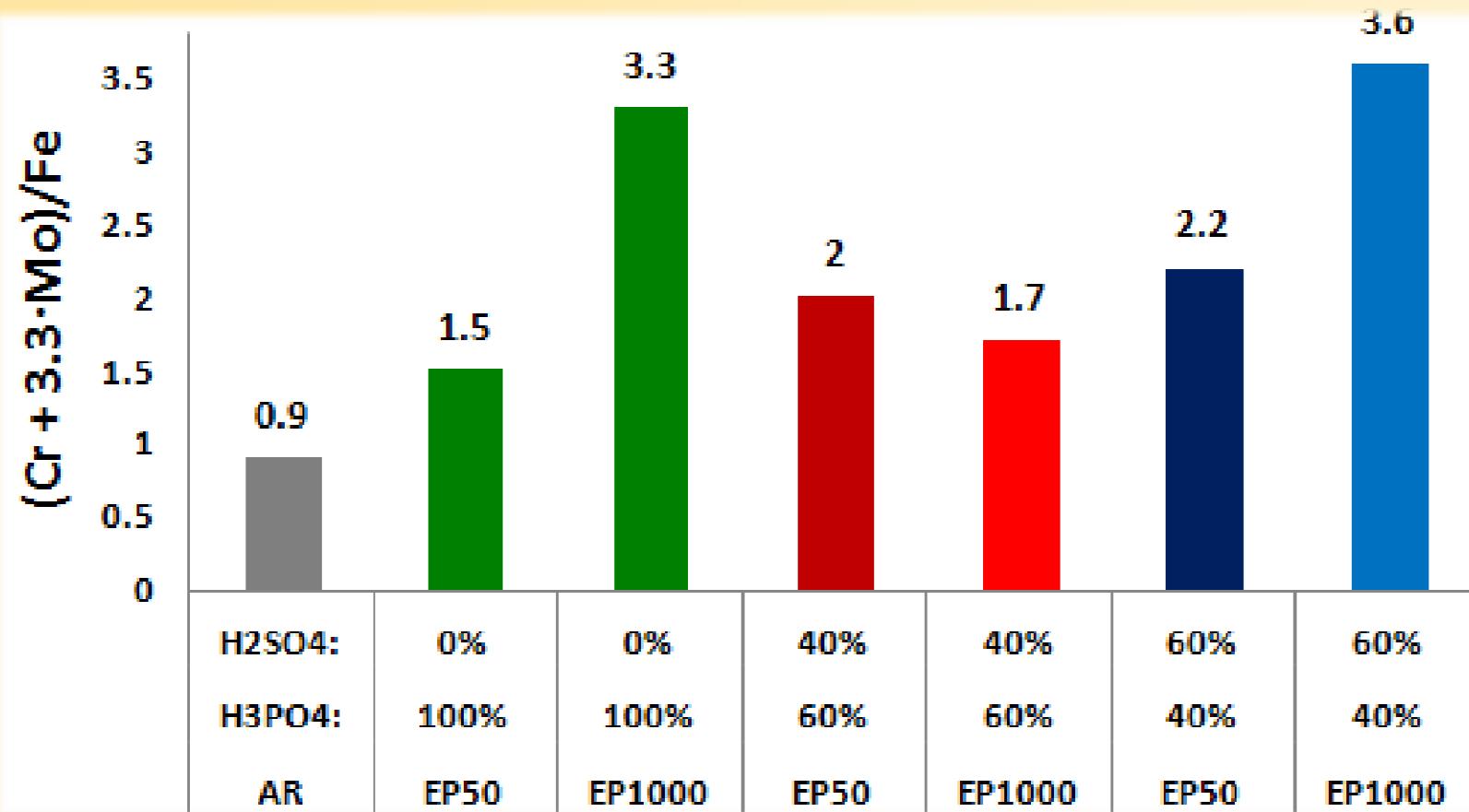
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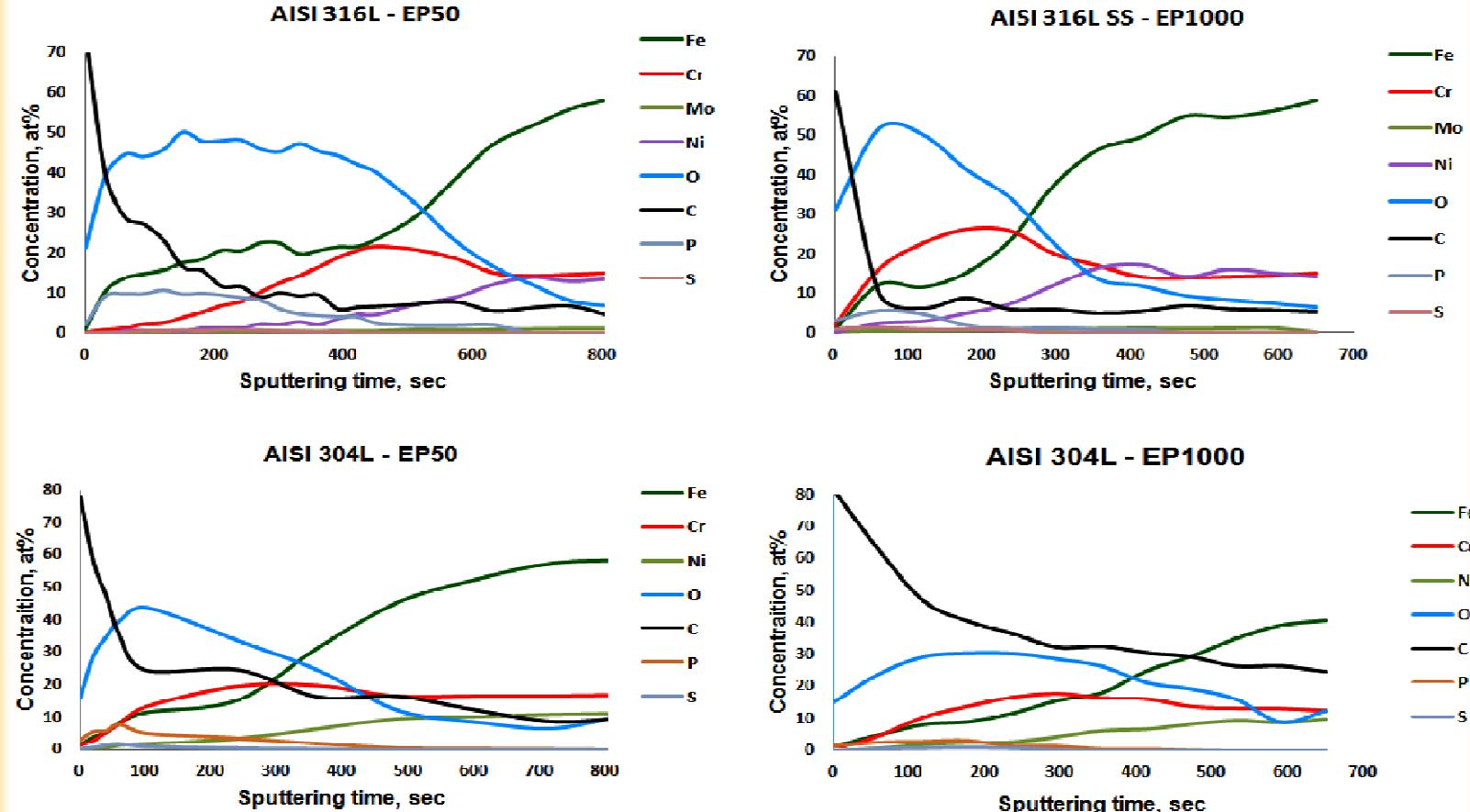
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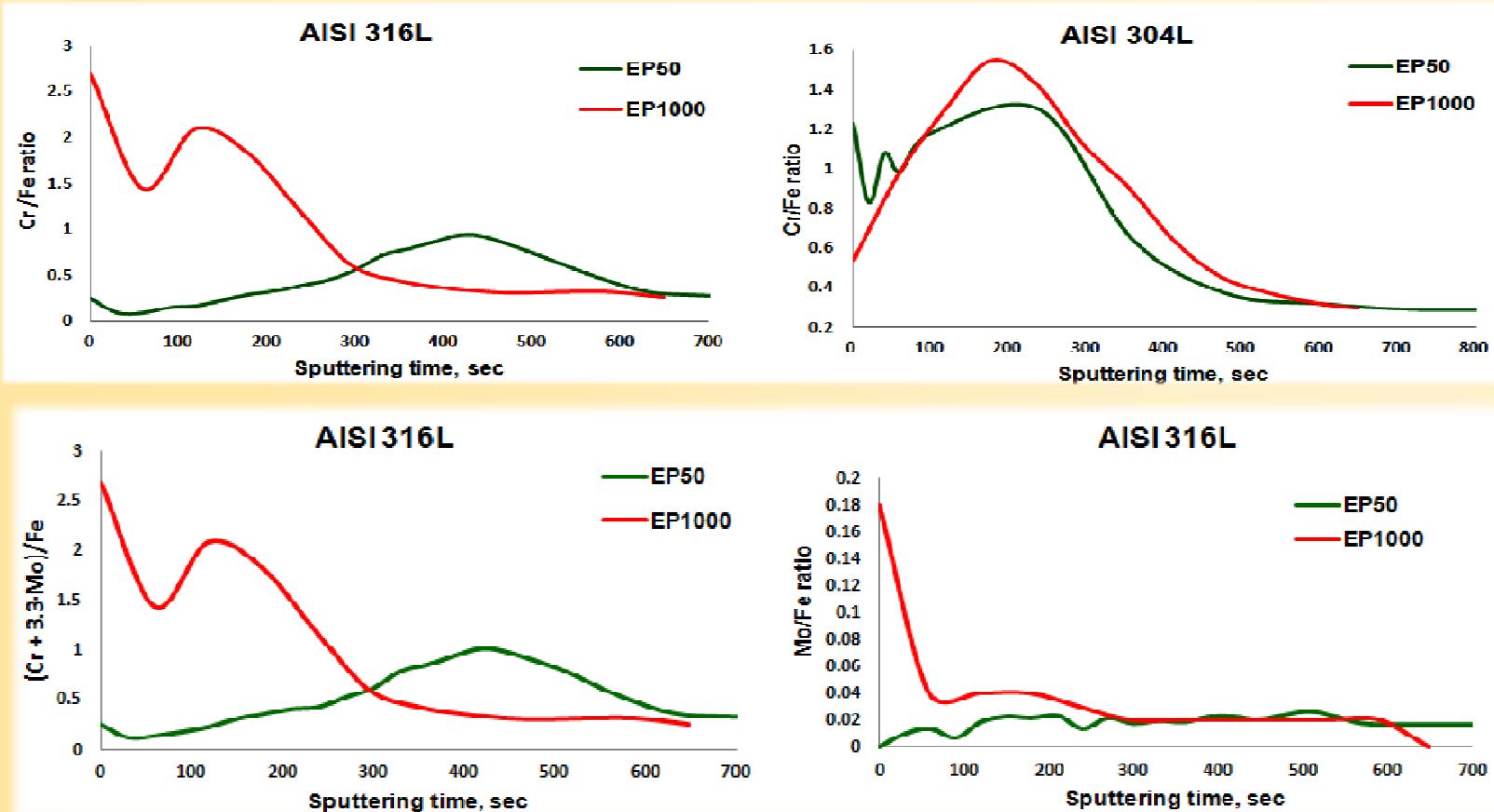
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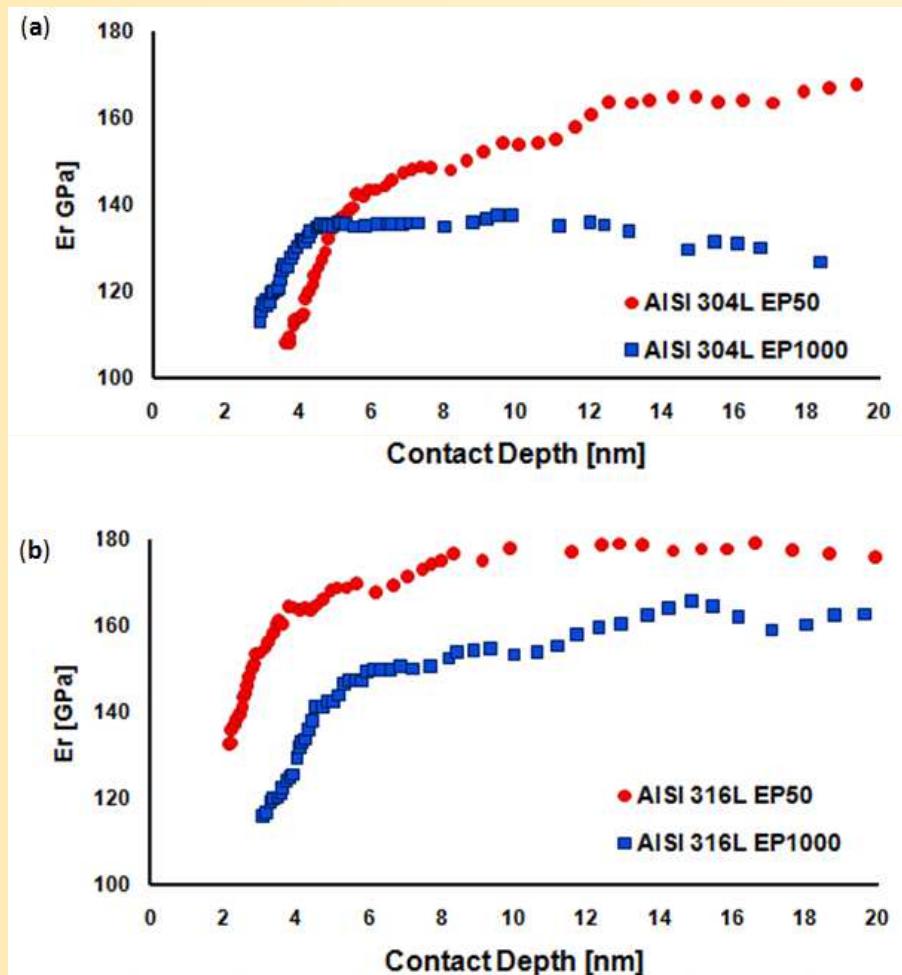
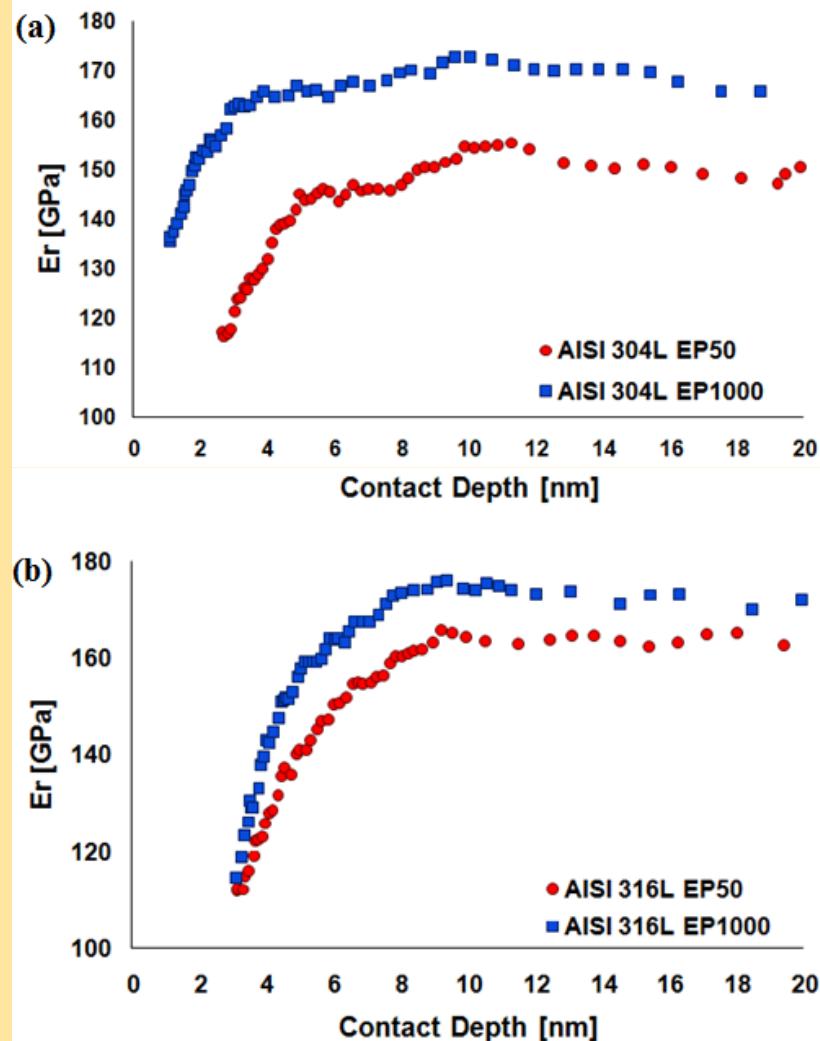
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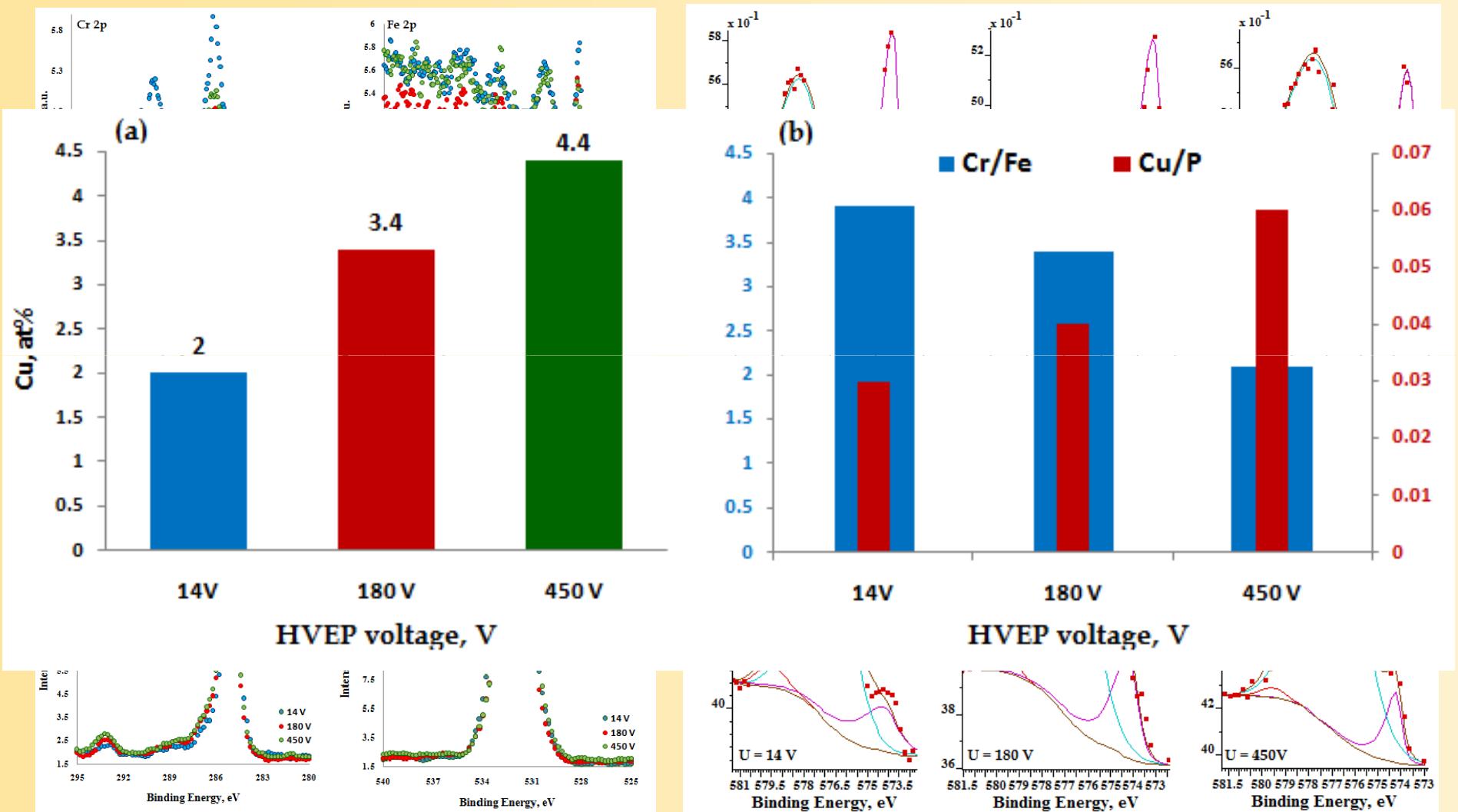
HIGH-CURRENT DENSITY ELECTROPOLISHING



NANONDENTATION



EP - AISI 304L SS



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T. Hryniewicz



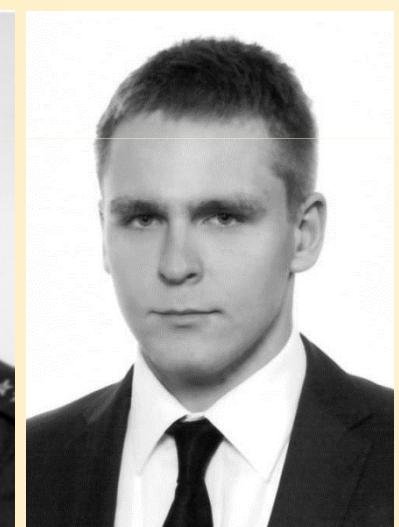
K. Rokosz



Ł. Dudek



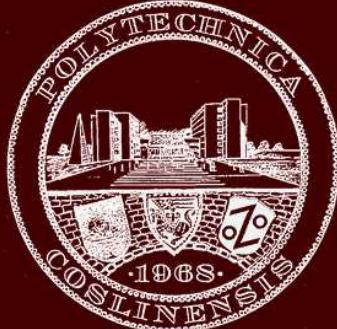
S. Rzadkiewicz



K. Pietrzak

PUBLICATIONS





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**THANK YOU
FOR ATTENTION**